

AN ALGORITHM TO DEVELOP LUMPED MODEL FOR GUNN-DIODE DYNAMICS

UMESH KUMAR

*Department of Electrical Engineering, I.I.T., Hauz Khas,
New Delhi- 110 016, India*

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A nonlinear lumped model can be developed for Gunn-Diodes to describe the diffusion effects as the domain travels from cathode to anode of a Gunn-Diode. The model describes the domain extinction and nucleation phenomena. It allows the user to specify arbitrary nonlinear drift velocity $V(E)$ and nonlinear diffusion $D(E)$.

The model simulates arbitrary Gunn-Diode circuits operating in any matured high field domain or in the LSA mode.

Here we have constructed an algorithm to lead to development of this model.

Keywords: Algorithm; lumped model; nonlinear dynamics; Gunn-Diode

INTRODUCTION

Nonlinearity is an inherent property of semi conductor devices. A device is called nonlinear when the relationship between its terminal variables namely voltage and current is other than linear. Modern device like the Gunn-Diode is strongly nonlinear. These devices exhibit complex dynamic behaviour.

With the leaping advances in integrated circuits the boundaries between circuit design and device design are becoming less recognizable. Therefore, in addition to the understanding of terminal behaviour of a device, it also becomes important to understand the interrelationship among physical processes, device geometry and terminal behaviour.

LUMPED NONLINEAR CIRCUIT MODEL

Let us take a 1-D structure of a Gunn-Diode of length L , area A , dielectric constant ϵ and a uniform donor concentration n_o . $n_o L > 10^{12}$ enables to support high field domains consisting of an accumulation layer with $n > n_o$ and a depletion layer with carrier concentration $n < n_o$. As the domain grows in size, it propagates from the cathode ($X = 0$) to the anode ($X = L$) with an instantaneous velocity $V_D(t)$.

Shapes of $n(x)$ and the field distribution (due to the dipole induction) $E(X)$ at different instants of time are governed by complex dynamics and affect device current and voltage.

DESCRIPTION OF THE MODEL

1. Cathode to anode capacitance:

$$C_1 = \frac{\epsilon A}{L} \quad (1)$$

2. Domain capacitance:

$$C_2 = \frac{\epsilon A}{W} \quad (2)$$

where W = Average domain width

$$= \frac{L}{T} \int_0^T |X_2(t) - X_1(t)| dt$$

3. Nonlinear Resistor: R with current I_R and Voltage V_R

$$I_R = G(V_R) = Aqn_o V(V_R/L) \quad (3)$$

where $V(E) = V(V_R/L)$ and $E = V_R/L$

4. Nonlinear current controlled source:

$$\begin{aligned} I_D &= I_D(V_1, V_2, I) \\ &= C_2 F(V_1, V_2) - I \end{aligned} \quad (4)$$

where

$$F(V_1, V_2) = n_o \left\{ \int_{V_1/L}^{E_m} \left| \frac{V(V_1/L) - V(E)}{n_a(E) - n_o} \right| dE + \int_{V_1/L}^{E_m} \left| \frac{V(V_1/L) - V(E)}{n_o - n_d(E)} \right| dE \right\} \quad (5)$$

$n_a(E)$, $n_d(E)$, E_m are found for each value of (V_1, V_2) as:

$$g(E_m; V_1, V_2) = 0 \quad (6)$$

$$g(E_m; V_1, V_2) = V_2 - \frac{\varepsilon}{q} \left\{ \int_{V_1/L}^{E_m} \frac{E - V_1/L}{n_a(E) - n_o} dE + \int_{V_1/L}^{E_m} \frac{E - V_1/L}{n_o - n_d(E)} dE \right\} \quad (7)$$

5. Accumulation layer carrier conc. $n_a(E)$:

For each given value of (V_1, V_2) , $n_a(E)$ is obtained by solving the following scalar nonlinear ordinary differential equation:

$$\frac{dn_a(E)}{dE} = Na(n_a, E; V_1, V_D) \quad (8a)$$

where with $D(E)$ being a nonlinear function of E , $Na(n_a, E; V_1, V_D) =$

$$\frac{n_a[V(E) - V_D] + n_o[V_D - V(V_1/L)] - q/\varepsilon(n_a - n_o)n_a D'(E)}{q/\varepsilon(n_a - n_o)D(E)} \quad (8b)$$

$$n_a(E) \big|_{E=E_o} = V_1/L = n_o \quad (8c)$$

$$n_a(E) \big|_{E=E_m} = n_o \quad (8d)$$

$V(D) = V_D(V_1, V_2)$ is domain velocity.

6. Depletion layer concentration: $n_d(E)$: For each given value of (V_1, V_2) , $n_d(E)$ is obtained by solving the initial value problem:

$$d \frac{n_d}{dE} = N_d(n_d, E; V_1, V_D) \quad (9a)$$

$$\begin{aligned} & \mathbf{N}_d(n_d, E; V_1, V_D) \\ &= \frac{n_d[V(E) - V_D] + n_o[V_D - V(V_1/L)] - (q/\varepsilon)(n_d - n_o)n_d D'(E)}{(q/\varepsilon)(n_d - n_o)D(E)} \end{aligned} \quad (9b)$$

where

$$n_d(E)|_{E=E_o} = V_1/L = n_o \quad (9c)$$

$$V(D) = V_D(V_1, V_2) \quad (9d)$$

V_D is already obtained from Eq. (8a) for given (V_1, V_2)

$n_d(E)$ depends on both V_1 and E and so $n_d(E) = n_d(E; V_1, E_m)$.

Eqs. (7), (8) and (9) are coupled together. Hence we must solve them as simultaneous equations by iterative methods.

Eq. (7) is only a scalar algebraic equations and can be solved by Newton-Raphson or the Secant method.

Once $n_a(E)$, $n_d(E)$ and E_m are found, the function $F(V_1, V_2)$ can be found by the help of the following algorithm:

$$\begin{aligned} & \text{Algorithm for Computing } F(V_1, V_2) \\ & \text{Given } (V_1, V_2) = (\bar{V}_1, \bar{V}_2) \end{aligned}$$

Step 1 Substitute (\bar{V}_1, \bar{V}_2) into Eqs. (7), (8) and (9).

Step 2 Assume two initial guesses $E_m^{(0)}$ and $E_m^{(1)}$

Step 3 Let $E_m = E_m^{(k)}$ and solve the two point boundary value problem (8) for

$$V_D = V_D^{(k)}(\bar{V}_1, \bar{V}_2) = V_D^{(k)}, \quad k = 0, 1 \quad (i)$$

$$\begin{aligned} n_a &= n_a(E; \bar{V}_1, E_m^{(k)}) \\ &= n_a^{(k)}(E), \quad k = 0, 1 \end{aligned} \quad (ii)$$

Step 4 Substitute (i) for VD in 9(b) with $k = 0$ and $k = 1$, respectively and solve the initial value problem for

$$n_d = n_d(E; \bar{V}_1, E_m^{(k)}) = n_d^{(k)}(E), \quad k = 0, 1 \quad (iii)$$

Step 5 Substitute (ii) and (iii) in (7) and solve for E_m^{k+1} using the following secant iteration formula:

$$E_m^{(j+1)} = E_m^{(j)} - F(E_m^{(j)})g(E_m^{(j)}, \bar{V}_1, \bar{V}_2) \quad (\text{iv})$$

where

$$F(E_m^{(j)}) = \frac{E_m^{(j)} - E_m^{(j-1)}}{g(E_m^{(j)}, \bar{V}_1, \bar{V}_2) - g(E_m^{(j-1)}, \bar{V}_1, \bar{V}_2)} \quad (\text{v})$$

Step 6 Iterate steps (3) through (5) with the subscript 'k' replaced by j, j = 2, 3 ... until the iteration converges, namely

$$n_a^{(j)}(E) \longrightarrow n_a(E; \bar{V}_1, \bar{V}_2) \quad (\text{vi})$$

$$n_d^{(j)}(E) \longrightarrow n_d(E; \bar{V}_1, \bar{V}_2) \quad (\text{vii})$$

and

$$E_m^{(j)} \longrightarrow E_m^{(j)}(\bar{V}_1, \bar{V}_2) \quad (\text{viii})$$

Step 7 Substitute (vi), (vii) and (viii) for $n_a(E)$, $n_d(E)$ and E_m in Eq. (5) and compute the two integrals numerically to obtain the required $F(\bar{V}_1, \bar{V}_2)$.

References

- [1] Bulkman, P. J., Hobson, G. S. and Taylor, B. G. (1972). *Transferred Electron Devices*, Academic Press, New York.
- [2] Hartanagal, H. L. (1973). *Gunn Effect Logic Devices*, Heinemann Educational Books, London.
- [3] Hobson, G. S. (1974). *The Gunn Effect*, Clarendon Press, Oxford.
- [4] Gunshor, R. L. and Kak, A. C. (1972). "Lumped Circuit representation of Gunn-Diodes in domain mode", *IEEE Trans. Electron Devices*, **ED-19**, 765-770.
- [5] Kak, A. C. and Gunshor, R. L. (1973). "The Transient behaviour of high field dipole domains in transferred electron devices", *IEEE Trans. Electron Devices*, **ED-20**, 1-5.
- [6] Butcher, P. N. (1967). "The Gunn Effect", *Report on progress in physics*, **XXX**, (part. I), 47-148.