

# Determination of Surface Composition by X-ray Photoelectron Spectroscopy Taking into Account Elastic Photoelectron Collisions

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It is now well known that elastic photoelectron scattering in the surface region of solids cannot be ignored in the mathematical formalism of quantitative XPS. Elastic collisions may increase or decrease the photoelectron signal intensity, depending on the experimental configuration. Consequently, it is advisable to take into account these effects in calculations of the surface composition. In certain experimental geometries, the photoelectron intensity is practically unaffected by elastic scattering events (configurations defined by the so-called "Master Angle"), and in principle such geometries should be recommended for measurements. Unfortunately, they usually cannot be implemented in typical constructions of spectrometers. In the present paper, different procedures for estimating corrections for elastic scattering events are overviewed. The influence of these correction procedures has been illustrated on examples of AuAgCu and AuAgPdCu alloys. It turned out that elastic photoelectron collisions substantially decrease the signal intensities selected for analysis. However, they are diminished by roughly the same factor. As a consequence, the calculated surface composition is only slightly modified by the correction procedure. This effect may not be of general validity for all solids, and the algorithms for calculating the surface composition should have an option for including any elastic scattering effects. Further efforts are needed to improve the predictive formulas providing corrections for elastic scattering effects.

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## 1 Introduction

X-ray photoelectron spectroscopy (XPS) is presently one of the most versatile tools for studies of solid surfaces. Despite the fact that this technique was developed in the second half of 1960s, it is presently used in surface studies with increasing frequency. As indicated in recent work,<sup>1</sup> the number of studies in which this technique is used is steadily growing. Over the last decade, this number has roughly doubled, reaching 5469 in 2007. There are several reasons for the high popularity of the XPS technique. Firstly, it is applicable to a great variety of samples, particularly to nonconductors, in contrast to Auger electron spectroscopy. Secondly, considerable advances in nanotechnology require a tool that makes possible studies of solid surfaces in the nanometer range. Furthermore, we can now observe considerable progress in instrumentation.

Spectrometers with a scanning facility are now available, which makes possible the mapping of a particular chemical species at the surface. Finally, the quantification of XPS is considered to be reasonably reliable, since photoelectron emission is a one-electron process that can be described by theory with relatively good accuracy.

Much attention has been devoted to the problem of quantifying XPS. The status of quantification by 1974 had been extensively reviewed by Fadley *et al.*<sup>2</sup> These authors outlined a mathematical formalism associated with this technique, which in fact, after few modifications, has been used until today. An introduction to quantitative XPS can also be found in numerous later reviews<sup>3,4</sup> and monographs.<sup>5,6</sup>

A determination of the surface composition by XPS requires knowledge of a reliable and accurate theoretical model relating the photoelectron signal intensity with the concentration of atoms emitting considered photoelectrons. The commonly used formalism is based on several assumptions specifying the sample and assumptions related to photoelectron transport in

solids. We assume that the sample is ideally flat, so the emitted photoelectrons are not recaptured by any surface protrusions. Furthermore, it is expected to be amorphous or polycrystalline. Consequently, the observed signal intensities are not modified by diffraction, or forward-focusing. Finally, we expect that the sample composition has a uniform in-depth composition within the sampling depth of XPS. The X-rays are assumed to be attenuated negligibly in the analyzed region. The ionizing radiation is not reflected from the surface, and there are no refraction effects. Two further assumptions conveniently simplify the formalism. The photoelectron intensity is assumed to be attenuated exponentially, and the photoelectron trajectories are expected to be linear from the point of emission up to the sample surface. Certainly, the photoelectron trajectories may deviate from linearity due to elastic interactions with atoms of the solid; the last assumption was considered to be controversial even in early days of electron spectroscopies. In his theoretical analysis of the Auger-plasmon-satellite intensities, Feibelman<sup>7</sup> wrote: "... one should make some effort to account for deflection of escaping electrons by elastic scattering from ion cores". Fadley *et al.*<sup>2</sup> admitted that the influence of elastic electron scattering on the angular distribution of emitted electron is assumed to be negligible, but "... a slight smearing effect ... cannot be ruled out".

The importance of elastic scattering effects in quantitative XPS analysis was initially proved in a series of papers by Baschenko and Nefedov.<sup>8-10</sup> These authors indicated that photoelectron elastic scattering events have a non-negligible effect on the angular distribution of photoemission. Results published by Baschenko and Nefedov stimulated further studies of photoelectron transport in the surface region of solids. Early research, until 1989, was reviewed by Jablonski.<sup>11</sup> Similar reviews were also published more recently.<sup>4,12</sup>

Although presently an important role of elastic photoelectron collisions in quantitative XPS is commonly recognized, it is not a common practice to account for these effects in routine analysis. This problem is extensively discussed in the present work.

## 2 Theory

We start with a brief introduction to the common formalism of XPS in which elastic photoelectron scattering is neglected. The photoelectron signal intensity,  $dI_x$ , originating from a thin layer of thickness  $dz$  located at a depth  $z$  is given by

$$dI_x = TD_e F_x A \Delta \Omega N (d\sigma_x/d\Omega) \exp[-z/(\lambda_{in} \cos \alpha)] dz, \quad (1)$$

where  $T$  is the analyzer transmission function,  $D_e$  the detector efficiency,  $F_x$  the flux of incident X-rays,  $A$  the analyzed area,  $\Delta \Omega$  the solid acceptance angle of the analyzer,  $N$  the atomic density of a given element (number of atoms in unit volume),  $\alpha$  the detection angle with respect to the surface normal,  $\lambda_{in}$  the inelastic mean free path of analyzed photoelectrons (IMFP), and  $d\sigma_x/d\Omega_x$  the differential photoelectric cross section. The latter parameter has the following form:

$$d\sigma_x/d\Omega = \sigma_x W(\beta, \psi) = \sigma_x \frac{1}{4\pi} \left[ 1 - \frac{\beta}{4} (3\cos^2 \psi - 1) \right], \quad (2)$$

where  $\sigma_x$  is the total photoelectric cross section,  $W(\beta, \psi)$  the photoelectric cross section normalized to unity,  $\psi$  the angle between the direction of X-rays and the direction towards the analyzer, and  $\beta$  the asymmetry parameter.

If the area irradiated by X-rays is larger than the analyzed area, then the following approximate relation holds

$$A = A_0 / \cos \alpha, \quad (3)$$

where  $A_0$  is the area seen by the analyzer at the normal direction of analysis. Upon integration of Eq. (1) with respect to depth  $z$ , while taking into account Eq. (3), we obtain an expression describing the photoelectron signal intensity from a uniform semi-infinite solid,

$$I_x = TD_e A_0 F_x \Delta \Omega N \lambda_{in} (d\sigma_x/d\Omega). \quad (4)$$

The influence of photoelectron elastic collisions on the signal intensity is well described with two correcting factors,  $Q_x$  and  $\beta_{eff}$ , both modifying the photoelectron photoelectric cross section<sup>11,13</sup>

$$\begin{aligned} (d\sigma_x/d\Omega)_{corr} &= \sigma_x Q_x W(\beta_{eff}, \psi) \\ &= \sigma_x Q_x \frac{1}{4\pi} \left[ 1 - \frac{\beta_{eff}}{4} (3\cos^2 \psi - 1) \right]. \end{aligned} \quad (5)$$

Extensive compilations of these parameters are available in the literature.<sup>14</sup> However, these data refer to elemental solids, and thus are of limited use in practical analysis. Corrections  $Q_x$  and  $\beta_{eff}$  are also compiled in NIST database 82.<sup>15</sup> Although the NIST data are available for elements and compounds, they cannot be conveniently used in routine calculations of quantitative XPS. Several predictive formulas for  $Q_x$  and  $\beta_{eff}$  were proposed<sup>16-19</sup> which, in principle, are applicable to any solid. They originate from two procedures:

1. An analytical solution of the kinetic Boltzmann equation within the so-called transport approximation.<sup>16-18</sup>
2. A fit of analytical expressions to results of Monte Carlo simulations of photoelectron transport in solids.<sup>19</sup>

### 2.1 Kinetic Boltzmann equation

It has been shown<sup>16</sup> that the photoelectron signal intensity derived within the transport approximation can be described by the following formula:

$$I_x^{el} = Y_x \frac{\mu \omega \lambda_{tr}}{4\pi} \left[ (1-\omega)^{-1/2} H(\mu, \omega) - \frac{\beta}{4} (3\cos^2 \psi - 1) + \frac{\beta \omega}{16} (3\cos^2 \theta - 1) H(\mu, \omega) \int_0^1 \frac{x(H(x, \omega))}{x + \mu} (3x^2 - 1) dx \right], \quad (6)$$

where  $\theta$  is the angle between the direction of X-rays and the surface normal,  $\mu = \cos \alpha$ ,  $\lambda_{tr}$  is the transport mean free path,  $\omega$  is the single-scattering albedo,

$$\omega = \frac{\lambda_{in}}{\lambda_{in} + \lambda_{tr}}, \quad (7)$$

$H(x, \omega)$  is the Chandrasekhar function,<sup>20</sup> and

$$Y_x = TD_e F_x \Delta \Omega N \lambda_{in} \sigma_x (A_0/\mu). \quad (8)$$

The photoelectron elastic scattering influence on the signal intensity is fully described here by the transport mean free path. This parameter is related to the differential elastic scattering cross section,  $d\sigma_e/d\Omega$ . For an element, we have

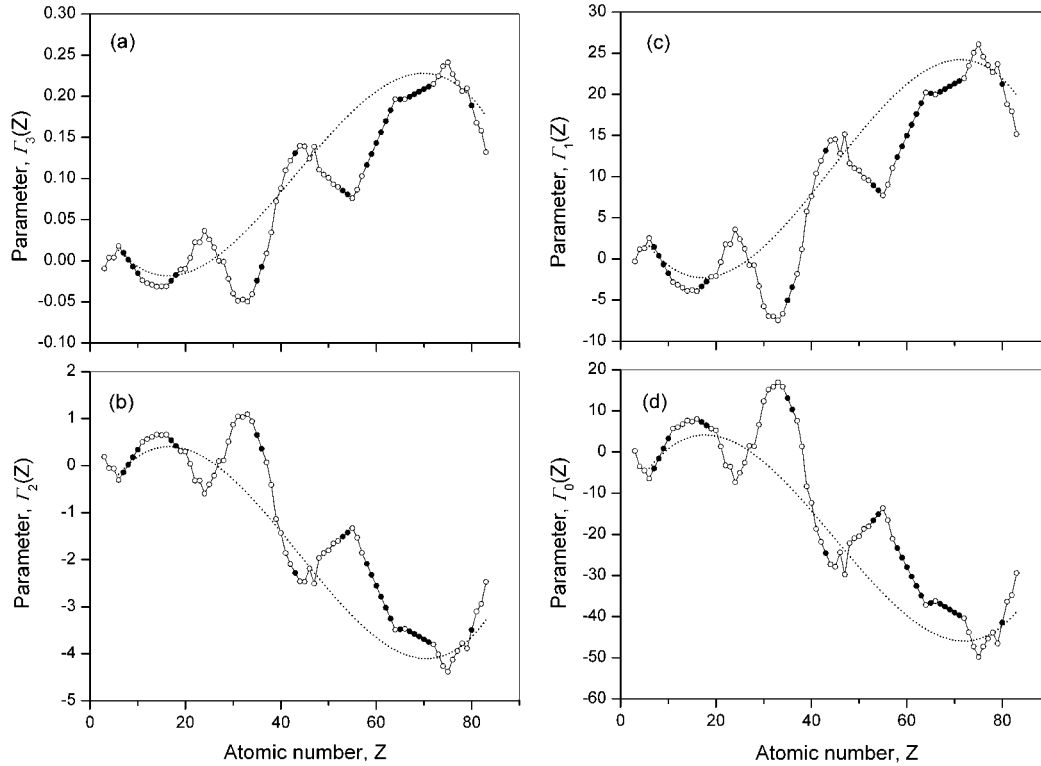


Fig. 1 Atomic number dependence of parameters  $\Gamma_k$ . Open circles, parameters calculated by fitting Eq. (16) to parameters  $\zeta$  calculated by Jablonski and Powell,<sup>18</sup> filled circles, parameters obtained by interpolation. A solid line is shown here to guide the eye. For a comparison, the atomic number dependence calculated in Ref. 17 is shown as a dotted line. (a) Parameter  $\Gamma_3(Z)$ , (b) parameter  $\Gamma_2(Z)$ , (c) parameter  $\Gamma_1(Z)$ , (d) parameter  $\Gamma_0(Z)$ .

$$\lambda_{tr} = \frac{1}{N\sigma_{tr}}, \quad (9)$$

where  $\sigma_{tr}$  is the transport cross section

$$\sigma_{tr} = 2\pi \int_0^\pi (1 - \cos \vartheta) \frac{d\sigma_e}{d\Omega} \sin \vartheta d\vartheta. \quad (10)$$

Equation (6) can be written in the form

$$I_x^{el} = TD_e A_0 F_x \Delta \Omega N \lambda_{in} \sigma_x Q_x \frac{1}{4\pi} \left[ 1 - \frac{\beta_{eff}}{4} (3\cos^2 \psi - 1) \right], \quad (11)$$

where

$$Q_x = \frac{\lambda_{tr}}{\lambda_{in} + \lambda_{tr}} (D_1 + D_2), \quad (12a)$$

$$\beta_{eff} = \frac{\lambda_{tr}}{\lambda_{in} + \lambda_{tr}} \frac{\beta}{Q_x}, \quad (12b)$$

$$D_1 = (1 - \omega)^{-1/2} H(\mu, \omega), \quad (12c)$$

$$D_2 = \frac{\beta\omega}{16} (3\cos^2 \theta - 1) H(\mu, \omega) \int_0^1 \frac{xH(x, \omega)}{x + \mu} (3x^2 - 1) dx. \quad (12d)$$

The term  $D_2$  was found to be considerably smaller than the term  $D_1$  and neglecting the term  $D_2$  affected the correction  $Q_x$  by less than 1%.<sup>16</sup> Consequently, Eq. (12a) - (12d) can be written as<sup>16,17</sup>

$$Q_x = (1 - \omega)^{1/2} H(\cos \alpha, \omega), \quad (13)$$

$$\beta_{eff} = \frac{(1 - \omega)\beta}{Q_x}, \quad (14)$$

$$\omega = \frac{1}{1 + \zeta}, \quad (15)$$

where  $\zeta$  is the ratio of the transport mean free path,  $\lambda_{tr}$ , to the inelastic mean free path,  $\lambda_{in}$ . We can see that the elastic scattering effects in quantitative XPS, within the formalism of the transport approximation, can be fully described by one parameter,  $\zeta$ . There are different methods for determining this parameter for a given solid from an analytical formalism. They are briefly reviewed below.

## 2-2 Algorithm of Jablonski

It has been postulated that the dependence of the ratio  $\zeta$  on the energy for any solid is well described by the following function:<sup>17,18</sup>

$$\zeta = \exp \left[ \sum_{k=0}^3 \Gamma_k (\ln E)^k \right], \quad (16)$$

where  $\Gamma_0$ ,  $\Gamma_1$ ,  $\Gamma_2$ , and  $\Gamma_3$  are fitted parameter characteristic for a given solid. This equation is a generalized form of an equation successfully used for describing the energy dependence of the IMFP,<sup>21</sup>

$$\lambda_{\text{in}} = cE^p = \exp(p \ln E + \ln c) = \exp(\Gamma_1 \ln E + \Gamma_0). \quad (17)$$

Jablonski<sup>17</sup> calculated the parameters  $\Gamma_k$  for 27 elements and for 22 energies in the range from 50 eV to 2 keV. The IMFPs were taken from Tanuma *et al.*<sup>22</sup> while the TMFPs were calculated for these elements using the relativistic partial wave expansion method (PWEM) under an assumption that the interaction between an electron and an atom of the solid follows the Thomas-Fermi-Dirac potential. It has been found that the dependence of the parameters  $\Gamma_k$  follows roughly a curve that is well approximated by a polynomial,

$$\Gamma_k = \Gamma_k(Z) = a_{k3}Z^3 + a_{k2}Z^2 + a_{k1}Z + a_{k0} = \sum_{n=0}^3 a_{kn}Z^n. \quad (18)$$

The fitted coefficients,  $a_{kn}$ , are available from Table 2 of Ref. 17. The resulting atomic number dependence of parameters  $\Gamma_k$  is shown in Figs. 1(a) - 1(d) as a dotted line. Introducing Eq. (18) into Eq. (16), we obtain a simple equation expressing the ratio  $\zeta$ :

$$\zeta = \exp \left[ \sum_{k=0}^3 \sum_{n=0}^3 a_{kn} Z^n (\ln E)^k \right]. \quad (19)$$

From the shape of the curves shown in Figs. 1(a) - 1(d), it follows that the coefficients  $\Gamma_k$  depend predominantly on the atomic number. Thus, we may generalize Eq. (19) to compounds, assuming that the weighted average of the atomic numbers can be introduced into this equation:

$$\bar{Z} = \sum_{i=1}^m x_i Z_i, \quad (20)$$

where  $m$  is the number of elements present in the sample, and the weight  $x_i$  the atom fraction of the  $i$ th element.

### 2.3 Algorithm of Jablonski and Powell

The ratios  $\zeta$  can be calculated using the coefficients  $\Gamma_k$  of improved accuracy. Jablonski and Powell<sup>18</sup> repeated the above analysis based on an extended set of the IMFPs and the TMFPs. The IMFP values were determined for 57 elements, partly from the optical data (34 elements), and partly from the predictive formula<sup>23</sup> (23 elements). For each element, 53 energies were considered; they were distributed roughly logarithmically in the energy range from 50 eV to 2 keV. For these elements and energies, the TMFP values were calculated from the relativistic PWEM calculations. Thus, in total, the analysis was founded on a set of 3021 ratios  $\zeta$ . The fit of Eq. (16) to this set provided, in the first step, the parameters  $\Gamma_k$ . They are plotted in Figs. 1(a) - 1(d). The numerical values of these parameters are compiled in Ref. 18 for atomic numbers from  $Z = 3$  to 83. We can now see that the dependences of parameters  $\Gamma_k$  on the atomic number are oscillating functions that cannot be approximated accurately by Eq. (18). It has been postulated to use tabulated parameters,  $\Gamma_k$ , in calculations of the ratios  $\zeta$  rather than to make an attempt to fit this dependence with a more sophisticated function than Eq. (18).

### 2.4 Algorithms of Seah and Gilmore

Seah and Gilmore<sup>19</sup> derived the predictive expressions for the  $Q_x$  and  $\beta_{\text{eff}}$  corrections from an extensive database of these parameters obtained by Jablonski<sup>14</sup> from the Monte Carlo simulations of photoelectron transport. The latter data were originally fitted by the following expressions<sup>13,14</sup>

$$\beta_{\text{eff}} = a_1 \cos^2 \alpha + a_2 \cos \alpha + a_3, \quad (21)$$

$$Q_x = b_1 \cos^2 \alpha + b_2 \cos \alpha + b_3, \quad (22)$$

where  $a_1$ ,  $a_2$ ,  $a_3$ ,  $b_1$ ,  $b_2$ , and  $b_3$  are the fitted coefficients. Extensive tabulations of these coefficients, for 27 elements and 396 photoelectron lines, are available in the literature.<sup>14</sup> Seah and Gilmore<sup>19</sup> proposed the following expression for  $Q_x$ :

$$Q_x = Q_x(0)(0.863 + 0.308 \cos \alpha - 0.171 \cos^2 \alpha), \quad (23)$$

where  $Q_x(0)$  is the value of  $Q_x$  for  $\alpha = 0$ .

$$Q_x(0) = 0.912 + 0.0148(Z + 16.21) \exp[-(Z + 16.21)/6.21] \\ + (3.07 \times 10^{-5} - 2.09 \times 10^{-7}Z)(E - 1200) \\ - (7.75 \times 10^{-8} - 1.45 \times 10^{-9}Z)(E - 1200)^2 \\ (E \text{ in eV}) \quad (24)$$

The expression for  $\beta_{\text{eff}}$  has a similar form,

$$\beta_{\text{eff}} = \beta_{\text{eff}}(0)(0.0868 \cos^2 \alpha - 0.208 \cos \alpha + 1.121), \quad (25)$$

where  $\beta_{\text{eff}}(0)$  is the value of  $\beta_{\text{eff}}$  for  $\alpha = 0$ .

$$\beta_{\text{eff}}(0)/\beta = 0.684 + 0.1005(Z + 6.47) \exp[-(Z + 6.47)/6.47] \\ + (1.598 \times 10^{-4} - 5.567 \times 10^{-6}Z \\ + 5.310 \times 10^{-8}Z^2)(E - 1200). \quad (26)$$

The parameters  $Q_x(0)$  and  $\beta_{\text{eff}}(0)$  can also be expressed in terms of the single scattering albedo,  $\omega$ :

$$Q_x(0) = (1 - \omega)^{1/2} \left[ 0.091 + \frac{2.684}{1 + 1.908(1 - \omega)^{1/2}} \right] \\ \text{for } \omega \geq 0.245, \quad (27a)$$

$$Q_x(0) = (1 - \omega)^{1/2} (1 + 0.412\omega) \quad \text{for } \omega < 0.245, \quad (27b)$$

$$\beta_{\text{eff}}(0) = 0.876\beta [1 - \omega(0.955 - 0.0777 \ln Z)]. \quad (28)$$

Equations (27) and (28) are considered to be more accurate than Eqs. (24) and (26).

Equations proposed by Seah and Gilmore<sup>19</sup> can in principle be generalized to compounds using the averaged atomic number (Eq. (20)). However, these authors recommended the following procedure for a given photoelectron line in a compound consisting of  $n$  elements:

$$Q_{\text{compound}} = \sum_{i=1}^n x_i [Q_x(\alpha)]_i, \quad (29a)$$

$$[\beta_{\text{eff}}/\beta]_{\text{compound}} = \sum_{i=1}^n x_i [\beta_{\text{eff}}(\alpha)/\beta]_i, \quad (29b)$$

where index  $i$  refers to pure elements. Equations (29a) and (29b) have obvious limitations in practical use. They cannot be applied to compounds in which one of the elements is gaseous, *e.g.* oxides or nitrides.

### 2.5 Separate expressions for the TMFP and the IMFP

The majority of predictive formulas for calculating the corrections  $Q_x$  and  $\beta_{\text{eff}}$  require knowledge of the single-scattering albedo,  $\omega$  (or the ratio  $\zeta$ ). In principle, these parameters can be calculated using separate predictive expressions for the TMFP and the IMFP. This approach seems to be presently the most accurate, although it is rather tiresome for routine use. Let us

first address the algorithm for calculating the TMFP. Several expressions were published in the literature.<sup>24-26</sup> We describe below the most recent formalism.<sup>26</sup>

For compounds or alloys consisting of  $m$  elements, the TMFP is related to the transport cross sections (TCS) of atoms constituting a given solid,

$$\lambda_{tr} = \left( N \sum_{i=1}^m x_i \sigma_{tr,i} \right)^{-1}, \quad (30)$$

where  $\sigma_{tr,i}$  is the TCS for the  $i$ th element, and  $N$  is the atomic density of a solid. For a given element, TCS can be calculated from an analytical expression consisting of two parts: (i) an analytical formula derived within the first Born approximation for the screened Rutherford potential,  $\sigma_{tr}^B$ , and (ii) a correcting function,  $G(\epsilon_0)$ .

$$\sigma_{tr} = \sigma_{tr}^B G(\epsilon_0), \quad (31)$$

where  $\epsilon_0$  is

$$\epsilon_0 = \frac{8mc_F^2 a_0^2}{\hbar^2} \frac{E}{(\mu^\infty)^2 Z^{2/3}} = 0.230440 \frac{E}{(\mu^\infty)^2 Z^{2/3}}, \quad (32a)$$

$$c_F = \frac{1}{2} \left( \frac{3\pi}{4} \right)^{2/3} = 0.8853414, \quad (32b)$$

$$\sigma_{tr}^B = \frac{32\pi Z^{2/3} c_F^4 a_0^2}{(\mu^\infty)^4} \frac{1}{\epsilon_0^2} \left[ \ln(1 + \epsilon_0) - \frac{\epsilon_0}{1 + \epsilon_0} \right], \quad (32c)$$

$$G(\epsilon_0) = \epsilon_0 \exp \left\{ \sum_{i=0}^4 A_i \left[ \ln(10\epsilon_0) \right]^{i/2} \right\}, \quad (32d)$$

where  $A_i$ ,  $0 \leq i \leq 4$  are fitted coefficients. These coefficients are available for all elements, and for two energy ranges: from 50 to 300 eV, and from 300 eV to 30 keV.<sup>26</sup> It has been shown that the mean deviation between the accurate TCS and the TCS resulting from Eq. (31) varies between 0.01 and 0.5%, depending on element. Thus, the accuracy of the above formalism is rather high, between two and four decimal digits.

The TPP-2M predictive formula for calculating the IMFP has the form<sup>23</sup>

$$\lambda_{in} = \frac{E}{E_p^2 [\beta \ln(\gamma E) - (C/E) + (D/E^2)]}, \quad (33)$$

where  $E$  is the electron energy (in eV), and

$$E_p = 28.8(N_v \rho / M)^{1/2} \quad (34a)$$

$$\beta = -0.10 + 0.944/(E_p^2 + E_g^2)^{1/2} + 0.069\rho^{0.1}, \quad (34b)$$

$$\gamma = 0.191\rho^{-0.50}, \quad (34c)$$

$$C = 1.97 - 0.91U, \quad (34d)$$

$$D = 53.4 - 20.8U, \quad (34e)$$

$$U = N_v \rho / M = E_p^2 / 829.4. \quad (34f)$$

In Eqs. (34a) – (34f),  $N_v$  is the number of valence electrons per atom or molecule,  $\rho$  the material density (in g/cm<sup>3</sup>),  $M$  the atomic or molecular weight, and  $E_g$  the band-gap energy (in eV). The input parameters for calculating the IMFP from Eqs. (33) – (34) are:  $E$ ,  $N_v$ ,  $E_g$  and  $\rho$ . The recommended values

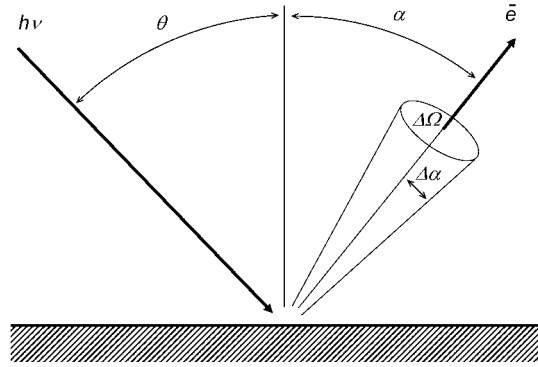


Fig. 2 Notation defining the XPS configuration. Note that the angle  $\theta$  becomes negative if the direction of X-rays and the analyzer axis are located on the same side of the surface normal.

of  $N_v$  for all elements are available in published tabulations.<sup>27,28</sup> These values can be used for estimating the  $N_v$  value for a given compound. The band-gap energy,  $E_g$ , for conductors is equal to zero. For other solids, some values are available in the literature. The rough guidance for estimating these values is published in a manual for the NIST IMFP database.<sup>28</sup> Fortunately, the IMFP is not a strong function of  $E_g$ , so a rough estimation is sufficient.

### 3 Master Angle Approach

The introduction of correction parameters for the elastic scattering effects into the formalism of quantitative XPS certainly complicates the computational procedure. First, we address here a question whether there are certain XPS configurations in which the elastic scattering effects are minimized.

We consider an experimental configuration in which the direction of X-rays, the analyzer axis and the surface normal are located in one plane (Fig. 2). Let us calculate the photoelectron signal intensity dependence on the incidence angle of X-rays,  $\theta$ , for a constant emission angle,  $\alpha$ . For this purpose, we use two theoretical models, one with the photoelectron elastic scattering neglected, and the second with the elastic scattering accounted for. On comparing of Eqs. (4) and (11), we can see that the signal intensity is proportional to the photoelectric cross section corrected for elastic-scattering effects,  $(d\sigma_x/d\Omega)_{corr}$ , or uncorrected for these effects,  $(d\sigma_x/d\Omega)$ . The corrected photoelectric cross section is calculated using the parameters  $Q_x$  and  $\beta_{eff}$  obtained from Eqs. (21) and (22) using fitted coefficients of Jablonski.<sup>14</sup> The results of calculations for Cu 2p<sub>3/2</sub> photoelectrons are shown in Fig. 3. For some experimental geometries, the elastic scattering effects are significant. Figure 4 shows the ratio  $I_x^{el}/I_x^{nel}$  calculated for three photoelectron lines: Cu 2p<sub>3/2</sub>, Ag 3d<sub>5/2</sub> and Au 4f<sub>7/2</sub>. As one can see, this ratio varies between 0.83 and 1.74. We note, however, that there are certain XPS configurations, defined by angles  $\theta$  and  $\alpha$ , in which the signal intensity is identical for both theoretical models. The angle between the direction of X-rays and the analyzer axis for such configurations has been tentatively termed the “Master Angle”.<sup>13</sup> For the master angle, denoted by  $\psi_0$ , we have:  $I_x^{nel} = I_x^{el}$  where the superscript “nel” denotes the common formalism. Consequently,

$$W(\beta, \psi_0) = Q_x W(\beta_{eff}, \psi_0) \quad (35)$$

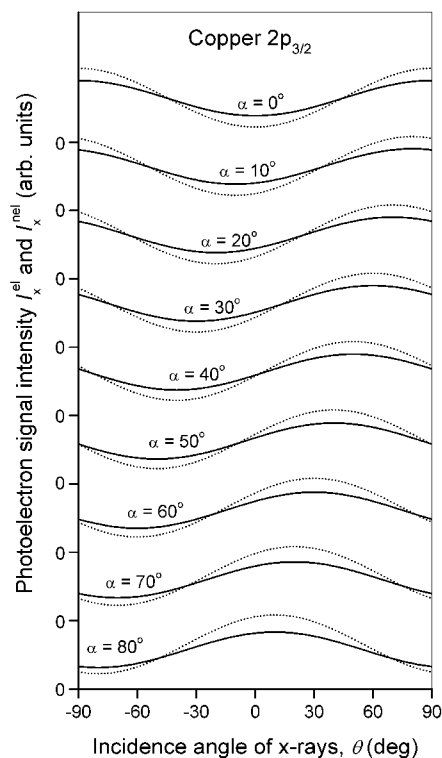


Fig. 3 Dependence of the photoelectron signal intensity on the incidence angle of X-rays,  $\theta$ , calculated for Cu  $2p_{3/2}$  photoelectrons for different emission angles,  $\alpha$  (Al  $K\alpha$  radiation). Solid line, intensity  $I_x^{\text{el}}$  calculated from the model that takes into account the elastic photoelectron scattering; dotted line, intensity  $I_x^{\text{nel}}$  calculated from the common formalism neglecting elastic scattering. Ticks on the ordinate axis indicate zero positions for consecutive plots.

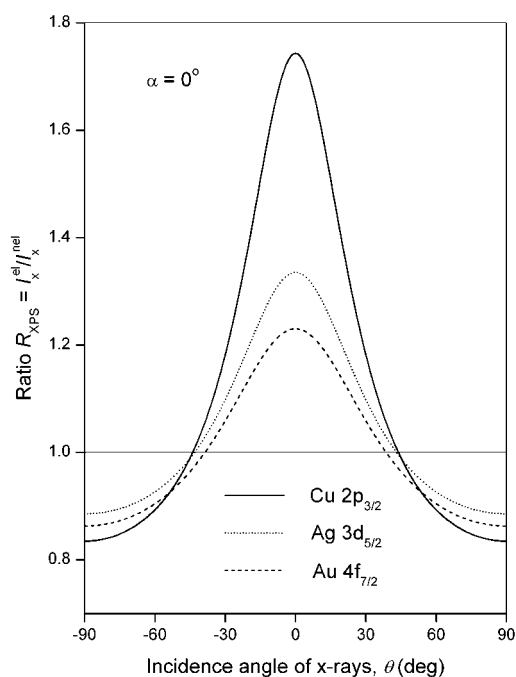


Fig. 4 Dependence of the ratio,  $R_{\text{XPS}} = I_x^{\text{el}}/I_x^{\text{nel}}$ , on the incidence angle of X-rays,  $\theta$ . Solid line, Cu  $2p_{3/2}$  photoelectrons; dotted line, Ag  $3d_{5/2}$  photoelectrons; dashed line, Au  $4f_{7/2}$  photoelectrons.

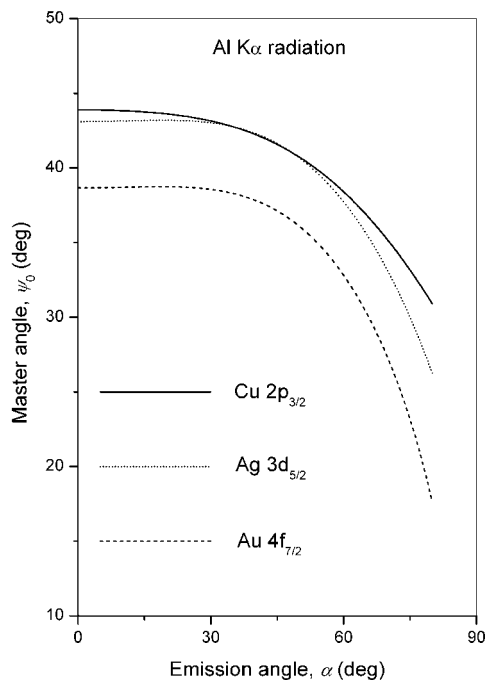


Fig. 5 Dependence of the master angle,  $\psi_0$ , on the photoelectron emission angle,  $\alpha$ . Solid line, Cu  $2p_{3/2}$  photoelectrons; dotted line, Ag  $3d_{5/2}$  photoelectrons; dashed line, Au  $4f_{7/2}$  photoelectrons.

and

$$\cos \psi_0 = \left[ \frac{1}{3} \left( 1 + \frac{4(1-Q_x)}{\beta - \beta_{\text{eff}} Q_x} \right) \right]^{1/2}. \quad (36)$$

In contrast to the “Magic Angle” [ $\psi_M = \arccos(3^{-1/2}) = 54^\circ 44' 8''$ ], the master angle is not a constant. Similarly as corrections  $Q_x$  and  $\beta_{\text{eff}}$ , the master angle depends on the photoelectron line, the emission angle of photoelectrons, and the solid. Figure 5 shows the emission angle dependence of the master angle for Cu  $2p_{3/2}$ , Ag  $3d_{5/2}$  and Au  $4f_{7/2}$  photoelectron lines calculated for the respective pure metals. In all cases, the master angle is considerably smaller than the magic angle. A similar observation was reported for different photoelectron lines in gold.<sup>13</sup>

If the master angles at a particular emission angle are identical for all photoelectron lines recorded for a given sample, then the simplest way to account for elastic scattering is to perform measurements in such a geometry. However, such a coincidence cannot be expected to be a rule. The master angle is frequently smaller than  $40^\circ$ , and the relevant configuration is not typical in XPS spectrometers. In general, we need to apply one of the correction procedures described in earlier sections.

#### 4 Multiline Approach

In geometries in which large elastic scattering effects are found, we also expect that the surface composition calculated from the XPS formalism, in which the photoelectron elastic scattering is taken into account, differs noticeably from the composition calculated from the common formalism. The procedure of introducing corrections for photoelectron elastic scattering is demonstrated below for an example of procedure called multiline analysis.<sup>29,30</sup>

Let us consider a uniform sample consisting of  $n$  elements. Suppose that  $m_i$  photoelectron signal intensities were measured for the  $i$ th element. At least one photoelectron intensity is measured for an element present in the sample. Multiline analysis leads to surface composition, such that the calculated photoelectron intensities are closest to the measured intensities. We assume that the energy dependence of the IMFP for a given sample can be expressed by a simple relation resulting from the Bethe equation,

$$\lambda_{in} = h \frac{E}{\ln(\gamma E)} \quad (37)$$

where the coefficient  $h$  depends on a sample and the coefficient  $\gamma$  is constant for a wide class of materials. It has been found<sup>31</sup> that the latter coefficient is equal to 0.05359 for elements, 0.05046 for inorganic compounds, and 0.09554 for organic compounds. This coefficient averaged over all solids is equal to 0.06403.

Let us denote by  $I_i^k$  the  $k$ th photoelectron intensity due to the  $i$ th element. We have

$$I_i^k = TD_e A_0 F_x \Delta \Omega h \frac{E_i^k}{\ln(\gamma E_i^k)} (d\sigma_x/d\Omega)_i^k M x_i, \quad (38)$$

where  $M$  is the total atomic density of the sample, and  $x_i$  is the atom fraction. Equation (38) may be rewritten as

$$I_i^k = CD_i^k x_i, \quad (39)$$

where

$$C = F_x \Delta \Omega M h, \quad (40)$$

$$\begin{aligned} D_i^k &= S(E_i^k) \frac{E_i^k}{\ln(\gamma E_i^k)} (d\sigma_x/d\Omega)_i^k \\ &= S(E_i^k) \frac{E_i^k}{\ln(\gamma E_i^k)} (\sigma_x)_i^k W(\beta_i^k, \psi). \end{aligned} \quad (41)$$

The product  $S(E) = TD_e A_0$  is the spectrometer function associated with the properties of a given instrument. According to a multiline analysis model designated by MLA-2, the surface concentration of  $i$ th element is calculated from:<sup>30</sup>

$$x_i = \frac{y_i}{\sum_{i=1}^n y_i}, \quad (42)$$

where

$$y_i = \frac{\sum_{k=1}^{m_i} (I_i^k)^2 D_i^k}{\sum_{k=1}^{m_i} I_i^k (D_i^k)^2}. \quad (43)$$

Any algorithm for calculating the surface composition, taking into account elastic photoelectron scattering, becomes equivalent to solving a system of nonlinear equations. We look for concentrations that are initially unknown; however, to calculate the corrections  $Q_x$  and  $\beta_{\text{eff}}$ , we need to assume a certain composition. It has been found that the following iteration procedure is effective for correcting the multiline algorithm for elastic photoelectron collisions:

1. We calculate the surface composition using the uncorrected formalism (Eqs. (41) - (43)).

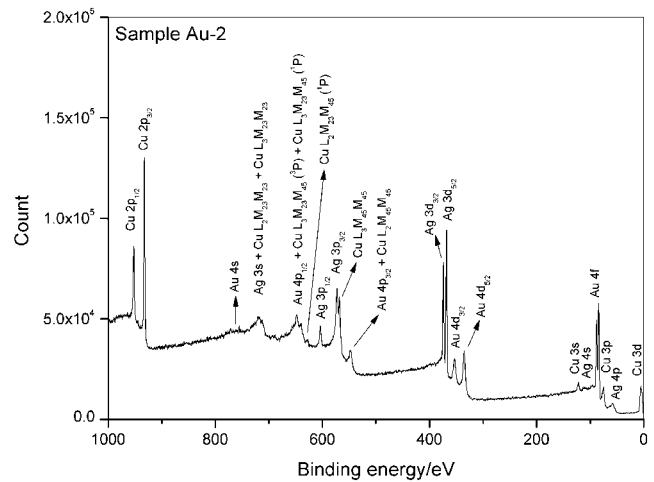


Fig. 6 Survey spectrum recorded for the Au-2 sample in the experimental configuration defined by angles  $\theta = 45^\circ$  and  $\alpha = 45^\circ$  (Al  $K_\alpha$  radiation).

2. For current surface concentrations,  $x_i$ , we calculate the average atomic number.
3. From one of the described above algorithms, we calculate corrections  $Q_x$  and  $\beta_{\text{eff}}$  for all measured photoelectron lines.
4. We calculate the parameters,  $D_i^k$  (Eq. (41)) modified as follows:

$$D_i^k = S(E_i^k) \frac{E_i^k}{\ln(\gamma E_i^k)} (\sigma_x)_i^k (Q_x)_i^k W[(\beta_{\text{eff}})_i^k, \psi]. \quad (44)$$

5. We calculate a new surface composition from Eqs. (42) and (43).
6. If the surface composition is different from the initial composition, we return to step No. 2 and repeat the calculations. Generally, the above iterations turn out to be quickly convergent.

## 5 Case Studies

In order to visualize the influence of photoelectron elastic scattering on the calculated composition, let us apply the described procedures of quantitative analysis to well-characterized samples. The samples used for that purpose were Certified Reference Materials for X-ray fluorescence spectrometry. They were manufactured and certified by Polish State Mint (Mennica, Metale Szlachetne). Two samples were submitted to analysis:

Au-2 sample: Au  $33.35 \pm 0.03$  wt%, Ag  $44.65 \pm 0.05$  wt%, and Cu  $21.98 \pm 0.05$  wt%,

Au-6 sample: Au  $49.99 \pm 0.07$  wt%, Ag  $12.54 \pm 0.05$  wt%, Cu  $12.53 \pm 0.05$  wt%, and Pd  $24.96 \pm 0.04$  wt%.

The alloys were prepared in the form of a thin foil, the thickness of which was close to 100  $\mu\text{m}$  deposited on an aluminium alloy support with a diameter of 30 mm.

The XPS spectra were recorded using a PHI 5000 VersaProbe<sup>TM</sup> spectrometer with monochromatic Al  $K_\alpha$  radiation. The X-ray beam was incident at the surface at  $\theta = 45^\circ$  with respect to the surface normal. The analyzer axis was located at  $\alpha = 45^\circ$  with respect to the surface normal. Consequently, the angle  $\psi$  was equal to  $90^\circ$ . For high-resolution spectra, the analyzer pass energy was 23.5 eV and the energy step size was 0.1 eV.

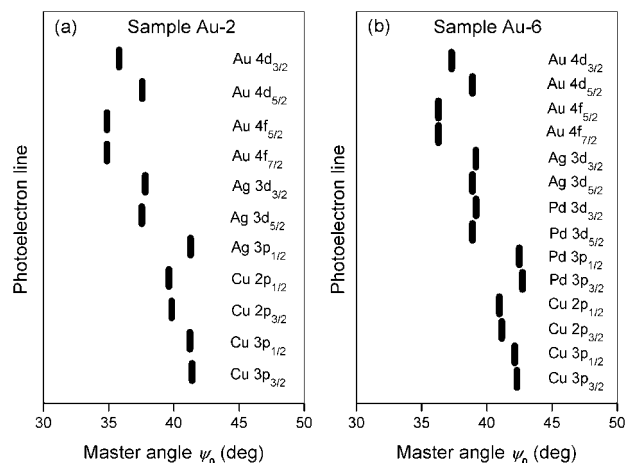


Fig. 7 Master angle values calculated for photoelectron lines recorded for the studied alloys. The bulk composition was assumed in calculations. (a) Alloy Au-2; (b) alloy Au-6.

The analyzer pass energy was 117.4 eV and the energy step size was 0.4 eV for recording the survey spectra. Prior to an XPS analysis, a sample area of 2 by 2 mm was cleaned for 2 min by argon ion sputtering. Ar<sup>+</sup> ions of energy 3 kV were incident at an angle of 55° with respect to the surface normal. After the cleaning procedure, the peaks due to contamination (carbon and oxygen) were no longer visible in the spectra. An exemplary survey spectrum for the Au-2 sample is shown in Fig. 6.

### 5.1 Master angles for studied alloys

From a spectrum recorded for the Au-2 sample, eleven photoelectron lines were selected for quantitative analysis and integrated (Cu 3p<sub>3/2</sub>, Cu 3p<sub>1/2</sub>, Cu 2p<sub>3/2</sub>, Cu 2p<sub>1/2</sub>, Ag 3p<sub>1/2</sub>, Ag 3d<sub>5/2</sub>, Ag 3d<sub>3/2</sub>, Au 4f<sub>7/2</sub>, Au 4f<sub>5/2</sub>, Au 4d<sub>5/2</sub> and Au 4d<sub>3/2</sub>). For the Au-6 sample, fourteen photoelectron lines were integrated (Cu 3p<sub>3/2</sub>, Cu 3p<sub>1/2</sub>, Cu 2p<sub>3/2</sub>, Cu 2p<sub>1/2</sub>, Pd 3p<sub>3/2</sub>, Pd 3p<sub>1/2</sub>, Pd 3d<sub>5/2</sub>, Pd 3d<sub>3/2</sub>, Ag 3d<sub>5/2</sub>, Ag 3d<sub>3/2</sub>, Au 4f<sub>7/2</sub>, Au 4f<sub>5/2</sub>, Au 4d<sub>5/2</sub> and Au 4d<sub>3/2</sub>). XPS spectra processing (background subtraction, peak fitting, integration) was performed using the software Advantage, version 4.30 (Thermo Fisher Scientific). The master angles were calculated from Eq. (36) using the corrections  $Q_x$  and  $\beta_{\text{eff}}$  determined for a given alloy assuming bulk composition. An algorithm of Jablonski and Powell<sup>18</sup> was used in calculations of the ratios,  $\zeta$ . The average atomic number was estimated from Eq. (20), and the needed coefficients,  $\Gamma_k$ , were taken from Ref. 18. The results of calculations are listed in Fig. 7. For the Au-2 alloy (Fig. 7(a)), the master angles were contained in a relatively narrow angular range, from 34.78° to 41.40°. If an XPS analysis could be made in a configuration determined by  $\psi_0$  equal to an intermediate angle (e.g. the value of 38.13° in the middle of angular range), we may expect that the elastic-scattering effects would be minimal. Unfortunately, such a geometry is not available in typical spectrometers.

Similar results were obtained for the alloy Au-6 (Fig. 7(b)). The master angles varied from 36.29° to 42.70°. The value in the middle of that range ( $\psi_0 = 39.5^\circ$ ) was very close to that obtained for the Au-2 alloy.

### 5.2 A measure for elastic scattering effects

The angle  $\psi$  for the PHI 5000 VersaProbe TM spectrometer used in measurements reported here is equal to 90°, and thus the influence of elastic photoelectron scattering on the signal

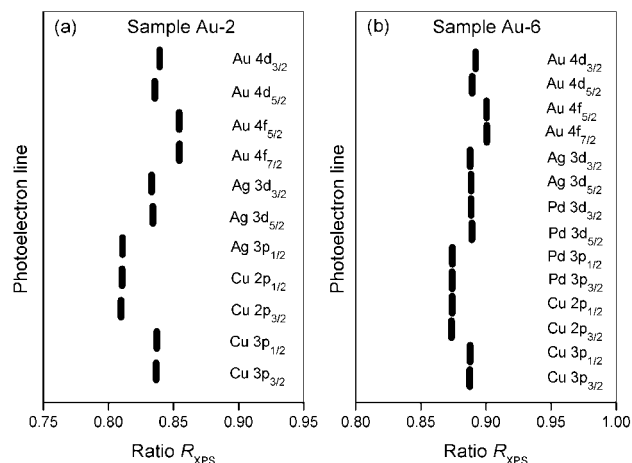


Fig. 8 The ratios  $R_{\text{XPS}}$  calculated for photoelectron lines recorded for the studied alloys. The bulk composition was assumed in calculations. (a) Alloy Au-2; (b) alloy Au-6.

intensity is non-negligible. As a simple measure of this influence, we can tentatively propose the ratio  $R_{\text{XPS}} = I_k^{\text{el}}/I_k^{\text{el}}$ . One can see in Fig. 4 that the elastic photoelectron collisions in the geometry of the measurements decrease the photoelectron intensity, and the decrease is the largest. For the selected three photoelectron lines, the ratio  $R_{\text{XPS}}$  varies between 0.835 and 0.886. These values refer to pure elements. Let us now calculate the ratios  $R_{\text{XPS}}$  for the analyzed alloys, assuming the bulk composition. Results obtained using the algorithm of Jablonski and Powell<sup>18</sup> for calculating  $I_k^{\text{el}}$  are shown in Fig. 8. For the Au-2 alloy, the ratio varies between 0.810 and 0.854, while for the Au-6 alloy it ranges from 0.874 to 0.901. The decrease in the photoelectron intensity due to elastic photoelectron collisions is significant in all cases. Note, however, that the decrease in the photoelectron intensity is very similar for all considered photoelectron lines, particularly for the Au-6 alloy (Fig. 8(b)). This is an important observation. If the photoelectron intensities vary by the same factor, then the surface concentrations calculated from any method involving relative sensitivity factors do not change. We may thus expect that the elastic photoelectron collisions only slightly affect the calculated concentrations of elements in the studied alloys.

### 5.3 Calculated surface composition

Two groups of photoelectron intensities were selected for calculations of the surface composition. In usual practice, we select the most pronounced line for each element. For the Au-2 alloy, as follows from Fig. 6, the Cu 2p<sub>3/2</sub>, Ag 3d<sub>5/2</sub> and Au 4f<sub>7/2</sub> lines are the most intense. Similarly, for the Au-6 alloy, we select the Cu 2p<sub>3/2</sub>, Pd 3d<sub>5/2</sub>, Ag 3d<sub>5/2</sub> and Au 4f<sub>7/2</sub> photoelectron lines. In the second group, all of the measured photoelectron lines were included.

The surface composition was calculated from a multiline approach. The concentrations of elements were calculated from an uncorrected formalism (Eqs. (41) – (43)), and also from the described iteration procedure to take into account the elastic photoelectron collisions. Parameters  $Q_x$  and  $\beta_{\text{eff}}$  were calculated from the algorithm of Jablonski<sup>17</sup> and from the algorithm of Jablonski and Powell.<sup>18</sup> Results of calculations are listed in Tables 1 and 2.

Several conclusions follow from these data. First, according to expectations, the surface concentrations are only slightly



Table 1 Surface composition of the reference alloy Au-2 obtained from the multiline algorithm

Method	Composition (mass fraction)		
	Cu	Ag	Au
Three most pronounced photoelectron lines: Cu 2p <sub>3/2</sub> , Ag 3d <sub>5/2</sub> and Au 4f <sub>7/2</sub>			
Elastic scattering neglected	0.250	0.347	0.403
Elastic scattering accounted	0.258	0.348	0.394
Algorithm of Jablonski <sup>17</sup>			
Elastic scattering accounted	0.258	0.348	0.394
Algorithm of Jablonski and Powell <sup>18</sup>			
Eleven photoelectron lines			
Elastic scattering neglected	0.263	0.358	0.379
Elastic scattering accounted	0.270	0.357	0.373
Algorithm of Jablonski <sup>17</sup>			
Elastic scattering accounted	0.270	0.357	0.373
Algorithm of Jablonski and Powell <sup>18</sup>			
Bulk composition	0.2198	0.4465	0.3335

Table 2 Surface composition of the reference alloy Au-6 obtained from the multiline algorithm

Algorithm	Composition (mass fraction)			
	Cu	Pd	Ag	Au
Four most pronounced photoelectron lines: Cu 2p <sub>3/2</sub> , Pd 3d <sub>5/2</sub> , Ag 3d <sub>5/2</sub> and Au 4f <sub>7/2</sub>				
Elastic scattering neglected	0.114	0.276	0.084	0.526
Elastic scattering accounted	0.117	0.279	0.085	0.519
Algorithm of Jablonski <sup>17</sup>				
Elastic scattering accounted	0.116	0.278	0.085	0.522
Algorithm of Jablonski and Powell <sup>18</sup>				
Fourteen photoelectron lines				
Elastic scattering neglected	0.129	0.289	0.096	0.486
Elastic scattering accounted	0.131	0.292	0.096	0.481
Algorithm of Jablonski <sup>17</sup>				
Elastic scattering accounted	0.131	0.291	0.096	0.483
Algorithm of Jablonski and Powell <sup>18</sup>				
Bulk composition	0.1253	0.2496	0.1254	0.4999

varied when the elastic scattering effects are taken into account. The largest percentage variation was observed for copper in the Au-2 alloy. The mass fraction changed from 0.250 (uncorrected formalism) to 0.258 (formalism corrected for elastic scattering), *i.e.* by 3.1%. For other elements the percentage changes were even smaller. Second, both algorithms used for correcting for elastic scattering effects provided the same results. Finally, the surface composition in all cases differed from the bulk composition, although the difference for the Au-6 alloy was not pronounced. In fact, this difference is comparable to differences resulting from different groups of photoelectron intensities used in calculations. The discrepancy between the bulk and surface concentration can be partially ascribed to selective sputtering; however, this effect is not analyzed here. One should also stress the fact that the calculated surface composition generally depends on the photoelectron lines selected for analysis. We may expect that results obtained from calculations, in which all

of the photoelectron lines were selected, are the most accurate.

## 6 Summary and Outlook

It should be mentioned here that the parameter  $R_{\text{XPS}}$  proposed as a measure of the elastic-scattering effects is closely related to the effective attenuation length (EAL) for determining the surface composition. EAL is defined as a “parameter which, when introduced in place of the IMFP into an expression derived for AES and XPS on the assumption that elastic-scattering effects are negligible for a given quantitative application, will correct that expression for elastic scattering effects”.<sup>32</sup> We have

$$R_{\text{XPS}} = I_{\text{x}}^{\text{el}}/I_{\text{x}}^{\text{nel}} = \frac{\lambda_{\text{in}} Q_{\text{x}} W(\beta_{\text{eff}}, \psi) W(\beta, \psi)}{\lambda_{\text{in}}} = \frac{L_{\text{QA}}}{\lambda_{\text{in}}}, \quad (45)$$

where  $L_{\text{QA}}$  is the EAL for quantitative analysis. We can see that  $L_{\text{QA}}$  approaches the IMFP when the elastic scattering effects are neglected.

As follows from Fig. 4, the largest percentage deviations between the photoelectron intensities, calculated from the common formalism and from a model taking into account the elastic-scattering effects, are expected for angles  $\psi$  smaller than 30°, especially in the region of  $\psi$  angles close to zero. Furthermore, for such geometries, the elastic scattering effects strongly depend on the photoelectron line. However, this is not a typical experimental configuration. There are only a few reports in which such a configuration was used.<sup>33-35</sup> It is obvious that, in such a configuration, the use of a formalism taking into account the elastic scattering effects is crucial.

Jablonski and Zemek<sup>35</sup> compiled the master angles for 396 photoelectron lines in 27 solids. They found that the master angles for different subshells are grouped in relatively narrow ranges. For example, the master angles for photoelectrons emitted from the f-subshells typically range from 36° to 40°. If the photoelectron lines in a studied solid have master angles in a relatively small range, then measurements in such a geometry may be recommended. Unfortunately, special constructions of spectrometers are needed for these measurements, for example spectrometers with a rotatable analyzer. When the sample is in the form of a thin foil, the preferable configuration would be such that the X-ray source and the analyzer are located on opposite sides of the foil.

In a typical XPS configuration, in which the angle  $\psi$  is equal to, or exceeds, the magic angle, some caution is advisable. Results presented here refer to two specific alloys only for which the elastic scattering effects are similar at  $\psi = 90^\circ$ . In general, the conclusions presented here may not be valid, and, for safety, it would be useful to check the influence of elastic scattering. As a guidance, we can use the algorithms presented here while assuming in calculations the bulk composition or the composition resulting from the formalism which neglected elastic scattering effects. It seems, however, that this is a fairly frequent occurrence that the decrease in the signal intensity due to elastic photoelectron collisions is comparable for the photoelectron lines recorded for a given sample. In consequence, a quantitative analysis of the surface composition by XPS, based on the typically used formalism, neglecting elastic scattering, is considered to be a very reliable technique.

On the other hand, we may encounter a situation in which one of the lines is affected more strongly by elastic scattering (*e.g.* due to distinctly different kinetic energy). Thus, the software packages for calculating the surface composition should have an option of including corrections for elastic scattering in

calculations of the surface composition. Such an extension is presently designed in the software package MULTI, implementing the multiline approach.<sup>30,36</sup> More effort should also be put to derive accurate and easy-to-use predictive formulas for the parameters  $Q_x$  and  $\beta_{\text{eff}}$ . Work on this problem is now in progress.<sup>37</sup> Finally, attention should be drawn to the fact that the reference database of parameters  $Q_x$  and  $\beta_{\text{eff}}$  was calculated using the elastic-scattering cross sections calculated for the Thomas-Fermi-Dirac potential.<sup>14</sup> It is now known that the cross sections calculated for the Dirac-Hartree-Fock potential are more accurate.<sup>38</sup> Thus, it would be useful to recalculate the reference data on  $Q_x$  and  $\beta_{\text{eff}}$  from a formalism that takes into account recent progress in the theory of electron transport. This work is planned for the near future.

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