一类非线性时滞系统的自适应模糊DSC控制

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摘 要 针对一类具有未知方向增益函数的严格反馈非线性时滞系统,提出了一种自适应模糊动态面 (Dynamic Surface Control) 控制算法.通过利用 DSC 设计技术和 Lyapunov-Krasovskii 函数,该算法不仅克服了计算膨胀的问题,而且同时补偿了未知的时滞.采用 Nussbaum 函数解决了虚拟控制增益的符号问题,并且避免了控制器的奇异性.所设计的控制器保证了闭环系统所有的状态和信号是半全局有界的,并且通过选择合适的设计参数可使跟踪误差为任意小.仿真结果表明了所提出控制器的有效性.

关键词 自适应控制,时滞,模糊系统,DSC

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Adaptive Fuzzy Dynamic Surface Control for a Class of Nonlinear Systems with Unknown Time-Delays

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Abstract In this paper, adaptive fuzzy dynamic surface control (DSC) is presented for a class of strict-feedback nonlinear systems with unknown time-delays and control directions. By incorporating DSC design technique and a novel Lyapunov-Krasovskii functions into adaptive fuzzy control design framework, the proposed control system can overcome not only the problem of "explosion of complexity" inherent in the backstepping design methods but also the unknown time-delays. The control singularity problem and unknown signs of the virtual control coefficients are well solved by use of Nussbaum gain function (NGF). The proposed controller guarantees the semiglobal boundedness of all states and signals in the closed-loop system, with arbitrary small tracking error by appropriately choosing design constants. Simulation results are given to demonstrate the effectiveness of the proposed scheme.

Key words Adaptive control, time-delay, fuzzy system, DSC

在过去的 20 年中, 自适应 backstepping 控制 成为了处理参数不确定性非线性系统的有力工具, 由此涌现出了许多卓有成效的成果^[1-6]. 文献 [3] 利用 Lyapunov 方程提出了一类严格反馈非线性 系统的自适应 backstepping 控制. 文献 [4] 提出 了基于二次 Lyapunov 方程的非线性系统自适应 神经网络 (NN) 控制, 此外, Yang 和 Zhou 利用 backstepping 和小增益理论设计了鲁棒自适应模糊 控制器^[5-6]. 但是, backstepping 设计方法有一个计 算膨胀 (explosion of complexity) 的缺陷, 这是由 于在每一步设计中都需要对非线性方程中的虚拟控 制进行重复求导,从而使得计算量较大. 文献 [7] 首 次提出了 DSC(dynamic surface control) 技术, 通 过引入一个一阶低通滤波器解决了此类问题.而后, 文献 [8] 利用 DSC 技术设计了一类参数严格反馈非 线性时滞系统的控制器. 同理, 针对纯反馈非线性 系统, Hou 等设计了鲁棒自适应模糊控制器^[9]. 许

多利用 DSC 技术的自适应控制系统同样被提出来 了^[10-12].

实际控制系统中普遍存在着时滞现象,通常我 们利用 Lyapunov-Krasovskii 方程或者 Lyapunov-Razumikhin 方程来补偿不确定系统的未知时滞^[13]. 为了处理未知的时滞和未知的虚拟控制符号,文献 [14-15] 提出了此类问题的解决方法.非线性时滞系 统的自适应神经控制也提出来了^[16-17].但是,以上 的文献中所设计的控制系统同样存在着计算膨胀的 问题^[16].如何使所设计的控制器具有简单的结构和 更少的自适应参数成为了一个具有挑战的课题,另 一方面,实际控制系统中的虚拟控制增益符号可能 未知, Nussbaum 增益函数可以处理此类问题^[18].

本文提出了一类非线性时滞系统的自适应模糊 动态面控制,基于万能逼近定理,模糊系统用来逼近 未知的非线性方程,通过 Lyapunov-Krasovskii 方 程可以得到控制律,同时未知的时滞也得以补偿. 对比目前存在的有关 DSC 控制方案,本文具有如 下优点:1)采用了一种新的 Lyapunov-Krasovskii 函数,有效的抵消了未知的时滞并且避免了控制器 出现奇异的可能性.2)由于所设计控制器中存在 Nussbaum 增益函数,在稳定性证明中运用了相

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关引理,从而使得稳定性证明过程简洁. 3)所提出 的自适应控制器具有更为简单的结构,并且包含更 少的自适应参数,从而减少了计算时间.该方案保证 了闭环系统所有的信号半全局一致有界,通过选择 合适的设计参数,可使稳态误差为任意小.

1 问题的提出

考虑如下的不确定非线性系统

$$\dot{x}_{i}(t) = f_{i}(\bar{\boldsymbol{x}}_{i}(t)) + g_{i}(\bar{\boldsymbol{x}}_{i}(t))x_{i+1}(t) + h_{i}(\bar{\boldsymbol{x}}_{i}(t-\tau_{i})) + d_{i}(t,\boldsymbol{x}) \quad 1 \leq i \leq n-1$$

$$\dot{x}_{n}(t) = f_{n}(\boldsymbol{x}(t)) + g_{n}(\boldsymbol{x}(t))u(t) + h_{n}(\boldsymbol{x}(t-\tau_{n})) + d_{n}(t,\boldsymbol{x})$$

$$\boldsymbol{x}(t) = \boldsymbol{\varphi}(t) \quad -\tau \leq t \leq 0$$
(1)

其中 $\bar{\boldsymbol{x}}_i(t) = [x_1, x_2, \cdots, x_i]^T$, $\boldsymbol{x} = [x_1, x_2, \cdots, x_n]^T \in \mathbf{R}^n$ 和 $u \in \mathbf{R}$ 分别是系统状态向量和控制输入. $f_i(\cdot), g_i(\cdot)$ 和 $h_i(\cdot)$ 是未知的平滑函数, $d_i(t, \boldsymbol{x}), i = 1, 2, \cdots, n$ 是外部有界干扰, τ_i 是未知的状态时滞, 且 $\tau_i < \tau_{max}, i = 1, 2, \cdots, n$. $\boldsymbol{\varphi}(t) \in \mathbf{R}^n$ 是状态变量的初始值. 控制目标是设计一个稳定的自适应控制器使系统 (1) 所有的信号半 全局有界. 为此, 对上述系统做如下的假设.

假设 1. 函数 $g_i(\mathbf{x})$ 的符号未知,且存在正的常数 g_0 和 g_m 使得 $0 < g_0 \le |g_i(\mathbf{x})| \le g_m < +\infty$.

假设 2. 存在正的未知连续函数 $\omega_i(\bar{\boldsymbol{x}}_i(t))$, 使得 $|d_i(t, \boldsymbol{x})| \leq \omega_i(\bar{\boldsymbol{x}}_i(t))$.

在自适应 DSC 设计中,首先引入误差面向量

$$e_1(t) = x_1(t)$$

 $e_i(t) = x_i(t) - \alpha_i(t) \ 1 \le i \le n$ (2)

其中 *i* = 1,...,*n*, *e_i*(*t*) 是第 *i* 个误差面, $\alpha_i(t)$ 是通过一阶滤波器得到的虚拟控制 律. *e_i*(*t*) = [*e*₁(*t*), *e*₂(*t*),...,*e_n*(*t*)]^T, *α_i*(*t*) = [$\alpha_1(t), \alpha_2(t), \cdots, \alpha_n(t)$]^T, $\alpha_1(t) = 0$.

假设 3. 时滞项 h_i(*x*_i(t)) 满足如下不等式:

$$|h_i(\bar{\boldsymbol{e}}_i(t) + \alpha_i(t))| \le \sum_{j=1}^i |\tanh(e_j(t))| q_{ij} \bar{\boldsymbol{e}}_j(t) \quad (3)$$

其中 $1 \leq i \leq n$, $q_{ij}\bar{e}_j(t)$ 为已知正定连续函数.

注 1. 假设 3 不同于文献 [8], [12] 等中提出 的关于时滞函数的假设,本文用 $tanh(e_j(t))$ 替代了 $e_j(t)$,一方面是由于计算简便的需要,另外,DSC 设计技术中需要用到滤波虚拟控制量 $\alpha_i(t)$ 来描 述误差 $e_i(t)$,又由于本文选择的 Lyapunov 函数为 $V_{0i} = \ln(\cosh(e_i))$,因此,根据以往的研究成果和本 文的需要,对假设 3 进行了合理的修改. 考虑系统(1)中存在的未知非线性,本文采用 模糊系统来进行逼近.根据万能逼近定理,可以把模 糊系统写为如下的形式:

$$F_i(\bar{\boldsymbol{x}}_i) = \boldsymbol{w}_i^{\mathrm{T}} \boldsymbol{P}_i(\bar{\boldsymbol{x}}_i) + \delta_i(\bar{\boldsymbol{x}}_i)$$
(4)

其中 \boldsymbol{w}_i 和 \boldsymbol{P}_i 分别是最优权向量和模糊基 函数, $\delta_i(\boldsymbol{x}_i)$ 是逼近误差,且 $|\delta_i(\boldsymbol{x}_i)| \leq \varepsilon_i, \varepsilon_i$ 为某一正常数. 理想的权向量 w^* 选为使 得 $\delta_i(\bar{\boldsymbol{x}}_i)$ 最小的 w. $\boldsymbol{P}_i(\boldsymbol{z}_i)$ 选为 $\boldsymbol{P}_i(\boldsymbol{z}_i) =$ $\prod_{i=1}^n \mu_{F_i}^{l_i}(\boldsymbol{z}_i) / \sum_{j=1}^N \prod_{i=1}^n \mu_{F_i}^{l_i}(\boldsymbol{z}_i)$.其中 $\mu_{F_i}^{l_i}(\boldsymbol{z}_i)$ 为 隶属函数.

下面介绍本文用到的 Nussbaum 型函数.

任意一个连续函数 $N(s) := \mathbf{R} \to \mathbf{R}$ 可以称作 是 Nussbaum 函数如果具有如下性质^[18].

$$\lim_{s \to \infty} \sup \frac{1}{s} \int_{0}^{s} N(\zeta) d\zeta = +\infty$$
$$\lim_{s \to \infty} \inf \frac{1}{s} \int_{0}^{s} N(\zeta) d\zeta = -\infty$$
(5)

本文中取 $N(\zeta) = \zeta^2 \cos(\zeta)$.

2 自适应模糊DSC系统设计

本小节具体设计控制器,控制器的设计包含 n步,在每一步中将设计虚拟控制律 α_{i+1} , $i = 1, 2, \cdots, n$.最后,在第n步时将会得到系统的控制律u.

步骤 1. 定义第一个误差面 $e_1 = x_1$,则有

$$\dot{e}_1 = f_1(x_1) + g_1(x_1)x_2 + h_1(x_1(t-\tau_1)) + d_1(t,x)$$
(6)

考虑如下的 Lyapunov-Krasovskii 函数 V01

$$V_{01} = \ln(\cosh(e_1)) + \sum_{i=1}^{n} \int_{t-\tau_i}^{t} Q_{i1}(e_1(\sigma)) d\sigma \quad (7)$$

其中正定函数定义为

$$Q_{i1}(e_1) = (n - i + 1) \frac{\tanh^2(e_1)}{2} q_{i1}^2(e_1)$$
 (8)

根据假设2和3,有以下的不等式成立:

$$\tanh(e_1)h_1(x_1(t-\tau_1)) \le \frac{\tanh^2(e_1)}{2} + \frac{\tanh^2(e_1(t-\tau_1))q_{11}^2(e_1(t-\tau_1))}{2} \quad (9)$$

$$\tanh(e_1)d_1(t,x) \le \frac{a_{11}^2}{2} + \frac{\tanh^2(e_1)\omega_1^2(x_1)}{2a_{11}^2} \quad (10)$$

其中 *a*₁₁ 是正的设计参数. 把 (8)-(10) 代入到 (7), 则有

$$\dot{V}_{01} \leq \tanh(e_1)[f_1(x_1) + \frac{\tanh^2(e_1)\omega_1^2(x_1)}{2a_{11}^2} + \frac{\tanh(e_1)}{2} + \frac{\tanh(e_1)}{2} \sum_{i=1}^n (n-i+1)q_{i1}^2(e_1)] + \\ \tanh(e_1)g_1(x_1)x_2 + \frac{a_{11}^2}{2} + \frac{\tanh^2(e_1(t-\tau_1))}{2} \times \\ q_{11}^2e_1(t-\tau_1) - \sum_{i=1}^n (n-i+1) \times \\ \frac{\tanh^2(e_1(t-\tau_i))}{2}q_{i1}^2e_1(t-\tau_i)$$
(11)

使 $\hat{F}_1(z_1) = f_1(x_1) + \tanh^2(e_1)\omega_1^2(x_1)/(2a_{11}^2) + \tanh(e_1)/2 + 1/2 \tanh(e_1)\sum_{i=1}^n (n-i+1)q_{i1}^2(e_1),$ 同时, 用模糊系统来逼近 $\hat{F}_1(z_1)$, 即

$$\hat{F}_1(z_1) = \boldsymbol{w}_1^{\mathrm{T}} \boldsymbol{P}_1(z_1) + \delta_1(z_1)$$
 (12)

其中 $|\delta_1(z_1)| \leq \varepsilon_1, \varepsilon_1$ 是一个正常数. 定义 $\hat{\theta}_i = ||w_i||^2,$ 如下的不等式成立:

$$anh(e_1) \boldsymbol{w}_1^{\mathrm{T}} \boldsymbol{P}_1(z_1) \leq rac{\hat{ heta}_1}{2\eta_1^2} \boldsymbol{P}_1^{\mathrm{T}}(z_1) \boldsymbol{P}_1(z_1) anh^2(e_1)
onumber \ + rac{\eta_1^2}{2}$$

$$\tanh(e_1)\delta_1(z_1) \le \frac{\tanh^2(e_1)}{2l_1^2} + \frac{l_1^2\varepsilon_1^2}{2} \qquad (13)$$

其中 η_1, l_1 为正的设计参数, 代入 (12)-(13) 到 (11), 得

$$\dot{V}_{01} \leq \frac{\hat{\theta}_{1} \tanh^{2}(e_{1})}{2\eta_{1}^{2}} \boldsymbol{P}_{1}^{\mathrm{T}}(z_{1}) \boldsymbol{P}_{1}(z_{1}) + \frac{\tanh^{2}(e_{1})}{2l_{1}^{2}} + \\ \tanh(e_{1})g_{1}(x_{1})x_{2} + c_{1} + \frac{\tanh^{2}(e_{1}(t-\tau_{1}))}{2} \times \\ q_{11}^{2}e_{1}(t-\tau_{1}) - \sum_{i=1}^{n}(n-i+1) \times \\ \frac{\tanh^{2}(e_{1}(t-\tau_{i}))}{2}q_{i1}^{2}e_{1}(t-\tau_{i})$$
(14)

其中 $c_1 = a_{11}^2/2 + \eta_1^2/2 + l_1^2 \varepsilon_1^2/2$. 选择如下的虚拟控制律 α_{2d}

$$\alpha_{2d} = N(\zeta_1)(k_1 \tanh(e_1) + \frac{\tanh(e_1)}{2l_1^2} + \frac{\theta_1}{2\eta_1^2} \boldsymbol{P}_1^{\mathrm{T}}(z_1)\boldsymbol{P}_1(z_1) \tanh(e_1))$$
(15)

$$\dot{\zeta}_{1} = k_{1} \tanh^{2}(e_{1}) + \frac{\tanh^{2}(e_{1})}{2l_{1}^{2}} + \frac{\theta_{1}}{2\eta_{1}^{2}} \boldsymbol{P}_{1}^{\mathrm{T}}(z_{1}) \boldsymbol{P}_{1}(z_{1}) \tanh^{2}(e_{1}) \qquad (16)$$

$$\dot{\theta}_1 = \frac{v_1}{2\eta_1^2} \boldsymbol{P}_1^{\mathrm{T}}(z_1) \boldsymbol{P}_1(z_1) \tanh^2(e_1) - v_1 \rho_1 \theta_1 \quad (17)$$

其中 $N(\zeta_1)$ 是平滑 Nussbaum-type 函数, k_1, v_1, ρ_1 为正常数, 让 α_{2d} 通过时间常数 $\kappa_2 > 0$ 的一阶低通 滤波器, 可得到滤波虚拟控制器 α_2 :

$$\kappa_2 \dot{\alpha}_2 + \alpha_2 = \alpha_{2d} \quad \alpha_2(0) = \alpha_{2d}(0) \tag{18}$$

定义系统边界误差 $y_2 = \alpha_2 - \alpha_{2d}$. 于是, 可得

$$\dot{y}_2 = -\frac{y_2}{\kappa_2} + B_2(e_1, y_2, \theta_1)$$
 (19)

其中 $B_2(e_1, y_2, \theta_1)$ 为一连续函数. 见本页底部. 把 $x_2 = e_2 + y_2 + \alpha_{2d}$ 代入到 (14), 对 (14) 进 行重新改写, 可得

$$\dot{V}_{01} \leq -k_1 \tanh^2(e_1) + \frac{\tilde{\theta}_1 \tanh^2(e_1)}{2\eta_1^2} \boldsymbol{P}_1^{\mathrm{T}}(z_1) \boldsymbol{P}_1(z_1) + (1 + g_1(x_1)N(\zeta_1))\dot{\zeta}_1 + c_1 + \tanh(e_1)g_1(x_1) \times (e_2 + y_2) + \frac{\tanh^2(e_1(t - \tau_1))}{2} q_{11}^2 e_1(t - \tau_1) - \sum_{i=1}^n (n - i + 1) \frac{\tanh^2(e_1(t - \tau_i))}{2} q_{i1}^2 e_1(t - \tau_i)$$
(21)

$$B_{2}(e_{1}, y_{2}, \theta_{1}) = -\frac{\mathrm{d}N(\zeta_{1})}{\mathrm{d}\zeta_{1}}\dot{\zeta}_{1}\left(k_{1} \tanh(e_{1}) + \frac{\theta_{1}}{2\eta_{1}^{2}}\boldsymbol{P}_{1}^{\mathrm{T}}(z_{1})\boldsymbol{P}_{1}(z_{1}) \tanh(e_{1}) + \frac{\tanh(e_{1})}{2l_{1}^{2}}\right) - N(\zeta_{1})\left(k_{1}\frac{\mathrm{d}\tanh(e_{1})}{\mathrm{d}e_{1}}\dot{e}_{1} + \frac{1}{2l_{1}^{2}}\frac{\mathrm{d}\tanh(e_{1})}{\mathrm{d}e_{1}}\dot{e}_{1}\right) - N(\zeta_{1})\left(\frac{\dot{\theta}_{1}}{2\eta_{1}^{2}}\boldsymbol{P}_{1}^{\mathrm{T}}(z_{1})\boldsymbol{P}_{1}(z_{1}) \tanh(e_{1}) + \frac{\theta_{1}}{2\eta_{1}^{2}}\left(\frac{\mathrm{d}\tanh(e_{1})}{\mathrm{d}e_{1}}\dot{e}_{1}\boldsymbol{P}_{1}^{\mathrm{T}}(z_{1})\boldsymbol{P}_{1}(z_{1}) + 2\boldsymbol{P}_{1}(z_{1})\frac{\partial\boldsymbol{P}_{1}(z_{1})}{\partial z_{1}}\dot{z}_{1}\right)\right)$$
(20)

其中 $\tilde{\theta}_i = \hat{\theta}_i - \theta_i, i = 1, 2, \cdots, n$. 利用如下的不等式:

$$\tanh(e_1)g_1(x_1)e_2 \le \frac{1}{4}\tanh^2(e_1) + g_1^2(x_1)e_2^2$$

$$\tanh(e_1)g_1(x_1)y_2 \le \kappa_2\tanh^2(e_1) + \frac{g_m^2y_2^2}{4\kappa_2} \quad (22)$$

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式(21)可进一步写为

$$\dot{V}_{01} \leq -(k_1 - \kappa_2 - \frac{1}{4}) \tanh^2(e_1) + (1 + g_1(x_1)N(\zeta_1))\dot{\zeta}_1 + \frac{\tilde{\theta}_1 \tanh^2(e_1)}{2\eta_1^2} \boldsymbol{P}_1^{\mathrm{T}}(z_1) \boldsymbol{P}_1(z_1) \\
+ c_1 + g_1(x_1)e_2^2 + \frac{g_m^2 y_2^2}{4\kappa_2} + \frac{\tanh^2(e_1(t - \tau_1))}{2} q_{11}^2 e_1(t - \tau_1) - \sum_{i=1}^n (n - i + 1) \\
\times \frac{\tanh^2(e_1(t - \tau_i))}{2} q_{11}^2 e_1(t - \tau_i) \quad (23)$$

注 2. 从式 (15) 可以看出虚拟控制器 α_{2d} 不包 含时滞项 $q_{ij}^2(e_j)$ 的任何信息, 这与文献 [8] 中设计 的控制器是不同的, 但注意 (23) 中的时滞项并没有 被抵消, 它将在最后一步的设计中才会被抵消. 下面 是步骤 2.

步骤 2. 定义第二个误差面 $e_2 = x_2 - \alpha_2$,则有

$$\dot{e}_2 = f_2(\bar{\boldsymbol{x}}_2) + g_2(\bar{\boldsymbol{x}}_2)x_3 + h_2(\bar{\boldsymbol{x}}_2(t-\tau_2)) + d_2(t, \boldsymbol{x}) - \dot{\alpha}_2$$
(24)

选择如下的 Lyapunov-Krasovskii 函数

$$V_{02} = V_{01} + \ln(\cosh(e_2)) + \sum_{i=2}^{n} \int_{t-\tau_i}^{t} Q_{i2}(\bar{e}_2(\sigma)) d\sigma \qquad (25)$$

则

$$\dot{V}_{02} = \dot{V}_{01} + \tanh(e_2)(f_2(\bar{\boldsymbol{x}}_2) + h_2(\bar{\boldsymbol{x}}_2(t - \tau_2)) + d_2(t, \boldsymbol{x})) + \sum_{i=2}^n \left(Q_{i2}(\bar{\boldsymbol{e}}_2) - Q_{i2}(\bar{\boldsymbol{e}}_2)(t - \tau_i) \right) + \tanh(e_2)g_2(\bar{\boldsymbol{x}}_2)x_3 - \tanh(e_2)\dot{\alpha}_2$$
(26)

和步骤 1 类似, 利用如 (9)-(10) 的不等式, 并选择 $Q_{i2}(\bar{e}_2)$ 为

$$Q_{i2}(\bar{\boldsymbol{e}}_2) = (n-i+1)\frac{\tanh^2(e_2)}{2}q_{i2}^2(\bar{\boldsymbol{e}}_2) \qquad (27)$$

则有

$$\dot{V}_{02} \leq \dot{V}_{01} + \tanh(e_2)\hat{F}_2(z_2) + \tanh(e_2)g_2(\bar{\boldsymbol{x}}_2)x_3 + \frac{a_{22}^2}{2} - \tanh(e_2)\dot{\alpha}_2 + \sum_{j=1}^2 \frac{\tanh^2(e_j(t-\tau_2))}{2} \times q_{2j}^2(\bar{\boldsymbol{e}}_j(t-\tau_2)) - \sum_{j=2}^n (n-j+1) \times \frac{\tanh^2(e_2(t-\tau_j))}{2} q_{2j}^2(\bar{\boldsymbol{e}}_2(t-\tau_j))$$
(28)

其中

$$\hat{F}_{2}(z_{2}) = f_{2}(\bar{\boldsymbol{x}}_{2}) + \frac{\tanh(e_{2})}{2} + \frac{\tanh(e_{2})}{2a_{22}^{2}}\omega_{2}^{2} + \frac{\tanh(e_{2})}{2}(n-i+1)q_{i2}^{2}(\bar{\boldsymbol{e}}_{2})$$
(29)

定义第三个误差面 $e_3 = x_3 - \alpha_3$, 用类似的推导 过程, 可得 $x_3 = e_3 + y_3 + \alpha_{3d}$. 选择虚拟控制器 α_{3d} 和自适应律为:

$$\alpha_{3d} = N(\zeta_2)[k_2 \tanh(e_2) + \frac{\tanh(e_2)}{2l_2^2} - \dot{\alpha}_2 + \frac{\theta_2}{2\eta_2^2} \boldsymbol{P}_2^{\mathrm{T}}(z_2) \boldsymbol{P}_2(z_2) \tanh(e_2)]$$
(30)

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$$\dot{\zeta}_{2} = k_{2} \tanh^{2}(e_{2}) + \frac{\tanh^{2}(e_{2})}{2l_{2}^{2}} - \tanh(e_{2})\dot{\alpha}_{2} + \frac{\theta_{2}}{2\eta_{2}^{2}}\boldsymbol{P}_{2}^{\mathrm{T}}(z_{2})\boldsymbol{P}_{2}(z_{2})\tanh^{2}(e_{2})$$
(31)

$$\dot{\theta}_2 = \frac{v_2}{2\eta_2^2} \boldsymbol{P}_2^{\mathrm{T}}(z_2) \boldsymbol{P}_2(z_2) \tanh^2(e_2) - v_2 \rho_2 \theta_2 \quad (32)$$

其中 $N(\zeta_2)$ 是平滑 Nussbaum-type 函数, k_2, ρ_2, v_2 为正常数. \dot{V}_{02} 可进一步写为

$$\begin{split} \dot{V}_{02} &\leq \sum_{i=1}^{2} \left(-(k_{i}-\kappa_{i+1}-\frac{1}{4}) \tanh^{2}(e_{i}) + \frac{\tilde{\theta}_{i} \tanh^{2}(e_{i})}{2\eta_{i}^{2}} + (1+g_{i}(\bar{\boldsymbol{x}}_{i})N(\zeta_{i}))\dot{\zeta}_{i} + c_{i} + g_{i}(\bar{\boldsymbol{x}}_{i})e_{i+1}^{2} + \frac{g_{m}^{2}y_{i+1}^{2}}{4\kappa_{i+1}} \right) + \sum_{i=1}^{2} \left[\sum_{l=i}^{2} (2-l+1) \times \frac{\tanh^{2}(e_{i}(t-\tau_{l}))}{2} q_{li}^{2}(\bar{\boldsymbol{e}}_{i}(t-\tau_{l})) - \sum_{l=i}^{n} (n-l+1) \times \frac{\tanh^{2}(e_{i}(t-\tau_{l}))}{2} q_{li}^{2}(\bar{\boldsymbol{e}}_{i}(t-\tau_{l})) \right] \qquad (33) \\ \mathbb{K} \div c_{i} = a_{ii}^{2}/2 + \eta_{i}^{2}/2 + l_{i}^{2}\varepsilon_{i}^{2}/2. \end{split}$$

步骤 k (3 $\leq k \leq n - 1$).利用类似的推导过程,并选择 Lyapunov-Krasovskii 为

$$V_{0k} = V_{0(k-1)} + \ln(\cosh(e_k)) + \sum_{i=k}^{n} \int_{t-\tau_i}^{t} Q_{ik}(\bar{e}_k(\sigma)) d\sigma$$
(34)

利用模糊系统和虚拟控制 $\alpha_{(k+1)d}$, 可得

$$\dot{V}_{0k} \leq \sum_{i=1}^{k} \left(-(k_{i} - \kappa_{i+1} - \frac{1}{4}) \tanh^{2}(e_{i}) + \frac{\tilde{\theta}_{i} \tanh^{2}(e_{i})}{2\eta_{i}^{2}} + (1 + g_{i}(\bar{\boldsymbol{x}}_{i})N(\zeta_{i}))\dot{\zeta}_{i} + c_{i} + g_{i}(\bar{\boldsymbol{x}}_{i})e_{i+1}^{2} + \frac{g_{m}^{2}y_{i+1}^{2}}{4\kappa_{i+1}} \right) + \sum_{i=1}^{k} \left[\sum_{l=i}^{k} (k - l + 1) \times \frac{\tanh^{2}(e_{i}(t - \tau_{l}))}{2}q_{li}^{2}(\bar{\boldsymbol{e}}_{i}(t - \tau_{l})) - \sum_{l=i}^{n} (n - l + 1)\frac{\tanh^{2}(e_{i}(t - \tau_{l}))}{2}q_{li}^{2}(\bar{\boldsymbol{e}}_{i}(t - \tau_{l})) \right]$$
(35)

步骤 n. 这一步实际控制 u 将得到,时滞项也 会被抵消掉. 根据 (1) 和 (2),可得

$$\dot{e}_n = f_n(\boldsymbol{x}) + g_n(\boldsymbol{x})u + h_n(\boldsymbol{x}(t-\tau_n)) + d_n(t,\boldsymbol{x}) - \dot{\alpha}_n$$
(36)

考虑 Lyapunov-Krasovskii 函数 V_{0n}

$$V_{0n} = V_{0(n-1)} + \ln(\cosh(e_n)) + \int_{t-\tau_n}^t Q_{nn}(\bar{\boldsymbol{e}}_n(\sigma)) d\sigma$$
(37)

选择 $Q_{nn}(e_n) = 1/2 \tanh^2(e_n)q_{nn}^2(e_n)$,利用类似 如 (9), (10) 的不等式和 (30)-(32),利用模糊系统 $\hat{F}_n(z_n)$ 来逼近未知函数,可以得出:

$$\dot{V}_{0n} \leq \sum_{i=1}^{n-1} \left(-(k_i - \kappa_{i+1} - \frac{1}{4}) \tanh^2(e_i) + \frac{\tilde{\theta}_i \tanh^2(e_i)}{2\eta_i^2} + (1 + g_i(\bar{\boldsymbol{x}}_i)N(\zeta_i))\dot{\zeta}_i + c_i + g_i(\bar{\boldsymbol{x}}_i)e_{i+1}^2 + \frac{g_m^2 y_{i+1}^2}{4\kappa_{i+1}} \right) + \frac{\hat{\theta}_n \tanh^2(e_n)}{2\eta_n^2} \times \boldsymbol{P}_n^{\mathrm{T}}(z_n)\boldsymbol{P}_n(z_n) + c_n + \frac{\tanh^2(e_n)}{2l_n^2} + \tanh(e_n)g_n(x_n)u$$
(38)

则实际的控制律 u 可以写为

$$u = N(\zeta_n)[k_n \tanh(e_n) + \frac{\tanh(e_n)}{2l_n^2} - \dot{\alpha}_n + \frac{\theta_n}{2\eta_n^2} \boldsymbol{P}_n^{\mathrm{T}}(z_n) \boldsymbol{P}_n(z_n) \tanh(e_n)]$$
(39)

参数的自适应律为

$$\dot{\zeta}_n = k_n \tanh^2(e_n) + \frac{\tanh^2(e_n)}{2l_n^2} - \tanh(e_n)\dot{\alpha}_n + \frac{\theta_n}{2\eta_n^2} \boldsymbol{P}_n^{\mathrm{T}}(z_n) \boldsymbol{P}_n(z_n) \tanh^2(e_n)$$
(40)

$$\dot{\theta}_n = \frac{v_n}{2\eta_n^2} \boldsymbol{P}_n^{\mathrm{T}}(z_n) \boldsymbol{P}_n(z_n) \tanh^2(e_n) - v_n \rho_n \theta_n \quad (41)$$

其中 k_n, v_n, ρ_n 是正的设计参数. 让 $\alpha_{(n+1)d}$ 通过时 间常数 $\kappa_{n+1} > 0$ 的一阶低通滤波器, 可得到滤波虚 拟控制器 $\alpha_{(n+1)}$:

$$\kappa_{n+1}\dot{\alpha}_{n+1} + \alpha_{n+1} = \alpha_{(n+1)d}$$

$$\alpha_{n+1}(0) = \alpha_{(n+1)d}(0)$$
(42)

显而易见, $x_{n+1} = u = \alpha_{(n+1)d}, \alpha_{n+1} = \alpha_{(n+1)d}.$

注 3. 从步骤 1 到步骤 *n* 的设计过程来看, 控制律 u(39) 的设计清晰明了,对比以往的文献 [8], [12] 等,本文的关键之处在于采用了一种新的 Lyapunov-Krasovskii 函数. 自适应律仅包含 2 个 参数 ζ_i 和 θ_i ,如果函数 $g_i(x)$ 的符号已知,我们仅需 要采用一个自适应律 θ_i 来设计控制器.

假设 4. 给定正常数 p,存在 $V(0) \le p$.

假设4表明了闭环系统所有的初始值是有界的, p的大小可根据初始值的大小进行调节.

下面提出如下定理.

定理 1. 考虑非线性时滞系统 (1) 满足假设 (1)-(4), 控制器 (39) 和自适应律 (40), (41) 保证了闭环 系统所有信号半全局一致有界, 并且误差可以为任 意小. 给定正常数 *p*, 初始值需满足

$$\sum_{j=1}^{n} e_j^2 + \sum_{j=1}^{n} \frac{1}{v} \tilde{\theta}_j^2 + \sum_{j=1}^{n} g_m^2 y_{j+1}^2 \le 2g_m p, \ \theta_i(t_0) \ge 0$$

证明.证明之前给出如下引理,引理1^[19]

1) 给定一任意有界函数 $g(\cdot) : \mathbf{R}^n \to \mathbf{R}$, 且 $C(\cdot) \in [-\varepsilon_0, \varepsilon_0]$, 则 $g(\cdot)N(\zeta)$ 是 Nussbaum 型函数, $N(\zeta) + C(\cdot)$ 同理也是 Nussbaum 型函数.

2) 使 V(t) 和 $\zeta(t)$ 为定义在 $[0, t_f)$ 上的平 滑函数且 $V(t) \geq 0$, $N(\zeta)\dot{\zeta}$ 为 Nussbaum 型函 数, ρ 是一个正常数, β 为常数. 如果 V(t) 满足 $\dot{V}(t) \leq -\rho V(t) + N(\zeta)\dot{\zeta} + \beta$, 则 V(t) 在 $[0, t_f)$ 上 是有界的. 首先考虑系统 (1) 为 1 阶的情况, 定义如下的 Lyapunov-Krasovskii 方程

$$V_1 = V_{01} + \frac{1}{2}g_m^2 y_2^2 + \frac{\tilde{\theta}_1^2}{2v_1}$$
(43)

根据 (23), 使 *n* = 1, 则

$$\dot{V}_{1} \leq -(k_{1} - \kappa_{1} - \frac{1}{4}) \tanh^{2}(e_{1}) + (1 + g_{1}(x_{1}) \times N(\zeta_{1}))\dot{\zeta}_{1} + \frac{\tilde{\theta}_{1} \tanh^{2}(e_{1})}{2\eta_{1}^{2}} \boldsymbol{P}_{1}^{\mathrm{T}}(z_{1}) \boldsymbol{P}_{1}(z_{1}) + c_{1} + g_{1}(x_{1})e_{2}^{2} + \frac{g_{m}^{2}y_{2}^{2}}{4\kappa_{2}} + g_{m}^{2}y_{2}\dot{y}_{2} - \frac{1}{v_{1}}\tilde{\theta}_{1}\dot{\theta}_{1} \quad (44)$$

把(18),(19)代入(44),并用如下的不等式

$$|y_2 B_2| \le \frac{y_2^2}{4\kappa_2} + \kappa_2 M_2^2, \ \tilde{\theta}_1 \theta_1 \le -\frac{\tilde{\theta}_1^2}{2} + \frac{\hat{\theta}_1}{2}$$

$$\frac{1}{2} \tanh^2(||\xi||) \le \ln(\cosh(||\xi||))$$
(45)

其中 M_2 是连续函数 $B_2(\cdot)$ 的极大值. 式 (44) 可进 一步写为

$$\dot{V}_{1} \leq -(k_{1} - \kappa_{2} - \frac{1}{4}) \tanh^{2}(e_{1}) - \frac{g_{m}^{2}y_{2}^{2}}{2\kappa_{2}} + C_{12} - \frac{\rho_{1}}{2}\tilde{\theta}_{1}^{2} + (1 + g_{1}(x_{1})N(\zeta_{1}))\dot{\zeta}_{1} + g_{1}(x_{1})e_{2}^{2} \leq -C_{11}[V_{1} - V_{Q_{1}}] + g_{1}(x_{1})e_{2}^{2} + C_{12} + (1 + g_{1}(x_{1})N(\zeta_{1}))\dot{\zeta}_{1}$$
(46)

其中 $C_{11} = \min\{2k_1 - 2\kappa_2 - 1/2, 1/\kappa_2, \rho_1 v_1\}, C_{12} = c_1 + g_m^2 \kappa_2 M_2^2 + \rho_1 \hat{\theta}_1^2/2, V_{Q_1} = \int_{t-\tau_i}^t Q_{i1}(e_1(\sigma)) d\sigma.$ 在式 (46) 中, $|\tanh(e_i)| < 1$, 函数 $q_{ij}(e_j)$ 是一个 有界函数, k_1 的选择需满足 $k_1 > \kappa_2 + 1/4, C_{11} > 0, C_{12} > 0.$ $(1 + g_1(x_1)N(\zeta_1))$ 可以看作是一个新的 Nussbaum 函数, 因此, 根据引理 1, 我们可以得出 如果 e_2 是有界的则 V_1 也是有界的.

同理, 最终的 Lyapunov-Krasovskii 函数可以 表示为

$$V_n = V_{0n} + \sum_{j=1}^n \left(\frac{1}{2}g_m^2 y_{j+1}^2 + \frac{1}{2v_j}\tilde{\theta}_j^2\right)$$
(47)

从 (42) 可知, $e_{n+1} = x_{n+1} - \alpha_{n+1} = 0$, $y_{n+1} = \alpha_{n+1} - \alpha_{(n+1)d} = 0$, 则

$$\dot{V}_{n} \leq -C_{n1}[V_{n} - \sum_{j=1}^{n} V_{Qj}] + g_{n}(x_{n})e_{n+1}^{2} + C_{n2} + (1 + g_{n}(x_{n})N(\zeta_{n}))\dot{\zeta}_{n}$$
(48)

其中 $C_{n1} = \min\{2k_n - 2\kappa_{n+1} - 1/2, 1/\kappa_{n+1}, \rho_n v_n\},$ $C_{n2} = c_n + g_m^2 \kappa_{n+1} M_{n+1}^2 + \rho_n \theta_n^2/2, V_{Q_j} = \int_{t-\tau_i}^t Q_{ij}(e_j(\sigma)) d\sigma.$ 根据引理 1 可知,如果 e_{n+1} 是 有界的则 V_n 也是有界的. 由于 $e_{n+1} = x_{n+1} - \alpha_{n+1} = 0$,所以 V_n 在有限时间内是有界的, e_n, y_n, θ_n 同样是半全局有界的. 同理进行 n-1 次 后推,显而易见 $V_i(t), e_i(t), y_{i+1}(t)$ 和 $\tilde{\theta}_i(t)$ 是一致 有界的,只要选择合适的参数 C_{n1}, p ,可使闭环系统 误差为任意小.

3 仿真结果及分析

仿真例一:考虑如下二阶非线性时滞系统:

$$\dot{x}_{1}(t) = f_{1}(x_{1}) + g_{1}(x_{1})x_{2}(t) + h_{1}(x_{1}(t-\tau_{1})) + d_{1}(t,x_{1})$$
$$\dot{x}_{2}(t) = f_{2}(\boldsymbol{x}) + g_{2}(\boldsymbol{x})u(t) + h_{2}(\boldsymbol{x}(t-\tau_{2})) + d_{2}(t,\boldsymbol{x})$$
(49)

其中 $f_1(x_1) = x_1(t)e^{-0.5x_1(t)}, f_2(x) = x_1(t)x_2^2(t),$ $g_1(x_1) = -(1 + x_1^2), \ g_2(x) = -(3 + \cos(x_1 x_2)),$ $h_1(x_1) = 2x_1^2, \ h_2(x) = 0.2x_2\sin(x_2), \ d_1(x_1) =$ $0.5x_1^2\cos(1.5t), d_2(x) = 0.5(x_1^2 + x_2^2)\sin(t).$ 为了 对比所提出算法的有效性,本仿真采用文献 [15] 中 的例子,并且加上了外界干扰 $d_1(t)$ 和 $d_2(t)$,同时 为了验证 Nussbaum 函数的有效性, 使函数 $g_i(x)$ 为严格负定. 模糊隶属函数 $\mu_{F_i}^l(x_i)$ 选为 $\mu_{F_i}^l(x_i) =$ $\exp(-(x_i + (0.8 - 0.2l))^2), l = 1, 2, \dots, 6.$ 选择如 下的初始值和参数: $[x_1(0), x_2(0)]^T = [-0.5, 1]^T$, $[\theta_1(0), \theta_2(0)]^{\mathrm{T}} = [\zeta_1(0), \zeta_2(0)]^{\mathrm{T}} = [0, 0]^{\mathrm{T}}, k_1 =$ $k_2 = 10, \ \eta_1 = \eta_2 = 0.5, \ l_1 = l_2 = v_1 = v_2 = 5,$ $\rho_1 = \rho_2 = 0.05, \kappa_2 = 0.001, \tau_1 = \tau_2 = 1,$ 采样时间 为 0.01s. 根据定理 1, 可得出如下的仿真结果, 图 1 为状态变量 x_1 和 x_2 的变化曲线. 图 2 为控制器 u, 图 3-5 分别为参数 θ 和 ζ 的自适应曲线. 由此可以 看出,闭环系统所有的信号都是有界的.从图中可以 看出,误差变量 $e_1 = x_1$ 在 t > 5s 后即趋于零. 控 制量 u 在 5s 之后基本趋于稳定, 对比文献 [15] 中 得出的控制量曲线,本文的控制输入无明显震荡.与 文献 [8] 提出的 DSC 控制算法相比, 由于采用了较 少的自适应律,相应的动态性能较好,各个参数都较 快的趋于稳定.



图 1 例 1 中状态变量 x_1 和 (实线) 和 $x_2(虚线)$ Fig. 1 State variables x_1 (solid line) and x_2 (dashed line) of example 1



图 2 例 1 中的控制量 *u* Fig. 2 The control input *u* of example 1







图 4 例 1 中自适应参数 $\zeta_1($ 实线) 和 $N(\zeta_1)($ 虚线) Fig. 4 Adaptive parameters ζ_1 (solid line) and $N(\zeta_1)$ (dashed line) of example 1





仿真例二:为了进一步验证所提出算法对高阶 系统的有效性,考虑如下三阶非线性时滞系统:

$$\dot{x}_{1}(t) = f_{1}(x_{1}) + g_{1}(x_{1})x_{2}(t) + h_{1}(x_{1}(t-\tau_{1})) + d_{1}(t,x)$$
$$\dot{x}_{2}(t) = f_{2}(\bar{x}_{2}) + g_{2}(\bar{x}_{2})x_{3} + h_{2}(\bar{x}_{2}(t-\tau_{2})) + d_{2}(t,x)$$
$$\dot{x}_{3}(t) = f_{3}(x) + g_{3}(x)u(t) + h_{3}(x(t-\tau_{3})) + d_{3}(t,x)$$
(50)

其中 $f_1(x_1) = x_1 \sin(x_1), g_1(x_1) = 0.5 + x_1^2,$ $f_2(\bar{x}_2) = x_2 e^{-0.1x_1}, g_2(\bar{x}_2) = 1 + x_2^2, f_3(x) =$ $x_1 x_2 x_3, g_3(x) = 2 + \cos(x_1), h_1(x) = x_1, h_2(\bar{x}_2) =$ $x_1 x_2, h_3(x) = x_2 x_3, d_1(t, x) = 0.5 x_1^2 \sin(t),$ $d_2(t, x) = x_1 x_2 \cos(t), d_3(t, x) = 0.5 \sin(t).$ 根据 定理 1, $e_1 = x_1, e_2 = x_2 - \alpha_2, e_3 = x_3 - \alpha_3.$ 模糊 基函数采用仿真 1 中的函数, 初始值和各个参数选 择如下: $[x_1(0), x_2(0), x_3(0)]^T = [0.1, -0.5, 0.5]^T$, $[\theta_1(0), \theta_2(0), \theta_3(0)]^T = [\zeta_1(0), \zeta_2(0), \zeta_3(0)]^T = [0, 0, 0]^T k_1 = 10, k_2 = k_3 = 1, \eta_1 = 0.1, \eta_2 = \eta_3 = 1, l_1 = l_2 = 1, l_3 = 10, v_1 = v_2 = 1, v_3 = 10, \rho_1 = \rho_2 = 1, \rho_3 = 0.5, \kappa_2 = \kappa_3 = 0.001, \tau_1 = 1, \tau_2 = 2, \tau_3 = 3.$ 采样时间设为 0.001s, 图 6-9 表明了仿真结果的有效性. 与文献 [12] 中三阶的例子相比,由于采用了较少的自适应参数, 控制输入和参数自适应曲线可较快的趋于平稳.



图 6 例 2 中状态变量 $x_1(实线), x_2(虚线)$ 和 $x_3(-.-)$ Fig. 6 State variables x_1 (solid line), x_2 (dashed line) and $x_3(-.-)$ of example 2



图 7 例 2 中的控制量 uFig. 7 The control input u of example 2



图 8 例 2 中自适应参数 $\theta_1($ 实线 $), \theta_2($ 虚线) 和 $\theta_3($ -.-)Fig. 8 Adaptive parameters θ_1 (solid line), θ_2 (dashed line) and $\theta_3($ -.-) of example 2



图 9 例 2 中自适应参数 $\zeta_1(实线), \zeta_2(虚线)$ 和 $\zeta_3(-.-)$ Fig. 9 Adaptive parameters ζ_1 (solid line), ζ_2 (dashed line)and $\zeta_3(-.-)$ of example 2

4 结论

本文研究了一类非线性时滞系统的自适应模糊 DSC 设计方法.模糊系统用来逼近未知的非线性 方程,基于 DSC 设计技术和 Nussbaum 函数,不仅 克服了自适应 backstepping 方法中固有的"计算膨 胀"的问题,而且不需要知道非线性不确定系统的控 制方向,通过利用 Lyapunov-Krasovskii 方程,未知 的时滞也得到了处理.和其他的方法对比,本方案结 构简单,计算量大大减少,并且具有更少的自适应调 节参数,外部的干扰也同时考虑进去了,更具有一般 的形式.仿真结果表明闭环系统所有的信号是半全 局有界的.

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